
CONTENTS
ABBREVIATIONS ..... III

1. INTRODUCTION ..... 1
2. EXISTING SITUATION ..... 3
2.1 Overview ..... 3
2.2 Structures ..... 3
2.3 Permanent Way ..... 8
2.4 Other Railway Facilities ..... 8
2.5 Utilities ..... 8
3. REQUIREMENTS ..... 10
3.1 Specific Requirements ..... 10
3.2 Systems Infrastructure and Integration ..... 10
3.3 Design Standards ..... 10
4. CONSTRAINTS ..... 12
4.1 Technical ..... 12
4.1.1 Electrical system ..... 12
4.1.2 Gauging ..... 15
4.1.3 Track Level ..... 15
4.1.4 Bridge Modification ..... 16
4.2 Environmental ..... 16
5. ELECTRICAL SOLUTION ASSESSMENT ..... 17
5.1 Electrical Case Hierarchy ..... 17
5.1.1 Risk Assessments ..... 21
5.2 Classification of Bridge Electrical Solutions ..... 22
5.2.1 Electrical solutions adopting a Nominal Contact Wire Height ( 4700 mm ) ..... 24
5.2.2 Electrical Solutions requiring a risk assessment ..... 25
5.2.3 Electrical Solutions requiring a derogation ..... 34
5.3 No Possible Electrical Solution ..... 39
6. BRIDGES REQUIRING INTERVENTION ..... 40
6.1 Bridges with an electrical solution requiring a derogation ..... 40
6.1.1 OBB 39 ..... 40
6.1.2 OBB 44 ..... 40
6.1.3 OBB 55 ..... 40
6.1.4 OBB 78 ..... 40
6.1.5 OBB 81 ..... 41
6.2 Bridges with no viable electrical solution in the existing arrangement ..... 41
6.2.1 OBB80/80A/80B ..... 41
APPENDIX A ..... 42
NTA
2040
Risk Assessments for Proposed Electrical Solutions where Contact Wire Height is less than 4700mm. 4243
Reports E1 to E6 ..... 43
FIGURES
Figure 4-1: Table 4.2.9.1. of the Energy Subsystem TSI ..... 13
Figure 4-2: Example of typical catenary support to contact wire with 500 mm droppers, passing under example bridge ..... 14
Figure 4-3: Example of typical contenary support showing achievement of a system height of 0mm underneath a reduced clearance bridge ..... 14
Figure 4-4: Example of pantographs clashing with bridge soffit ..... 15
Figure 5-1: General hazards associated with reduced contact wire heights at overbridges ..... 21
Figure 5-2: Hazards within stations associated with reduced contact wire heights at overbridges ..... 22
Figure 5-3: Hazards associated with reduced contact wire heights at overbridges designated for public use ..... 22
TABLES
Table 1-1: List of key documents associated with Electrification of the Northern Line from Malahide to Drogheda ..... 2
Table 2-1: Relevant information for clearance works to existing overbridges between Malahide and Drogheda ..... 4
Table 3-1: Relevant design standards for OHLE bridge clearance works ..... 10
Table 5-1: Electrical case hierarchy at overbridge structures ..... 18
Table 5-2: Summary of the proposed electrical solutions at each overbridge ..... 22
Table 5-3: Bridges with a proposed contact wire height of 4700 mm ..... 24
Table 5-4: Proposed electrical solution with $4500 \mathrm{~mm} \leq \mathrm{CWH}<4700 \mathrm{~mm}$ ..... 26
Table 5-5: Proposed electrical solution parameters with $4500 \mathrm{~mm} \leq \mathrm{CWH}<4700 \mathrm{~mm}$ ..... 27
Table 5-6: Proposed electrical solution with $4400 \leq$ CWH $<4500 \mathrm{~mm}$ ..... 30
Table 5-7: Proposed electrical solution parameters with $4400 \leq$ CWH $<4500 \mathrm{~mm}$ ..... 31
Table 5-8: Potential electrical solution with $4200 \mathrm{~mm}<\mathrm{CWH}<4400 \mathrm{~mm}$ (Derogation required) ..... 35
Table 5-9: Potential electrical solution parameters with CWH < 4400 mm (Derogation required) ..... 36

Coastal North

## ABBREVIATIONS

| Abbreviation | Definition |
| :--- | :--- |
| CAF | Common assessment framework |
| CCE | Chief Civil Engineer |
| CWH | Contact Wire Height |
| DC | Direct Current |
| EC | Electrical Case |
| FRS | Functional Requirements Specification |
| IÉ | larnród Éireann |
| MCA | Multi-criteria analysis |
| NIAH | National Inventory of Architectural Heritage |
| OHLE | Overhead line equipment |
| OLE | Overhead line electrification |
| SET | Signalling, electrification and telecoms |
| SH | Structural Height |
| ToR | Top of rail |
| TSS | Train Service Specification |

NTA $Q|=|$

## 1. INTRODUCTION

This report provides an update to the technical assessment of the overbridges between Malahide and Drogheda that was developed during Phase 2 (Concept, Feasibility and Options) to give a justification for why particular overbridges require clearance improvement works in order to facilitate feasible OHLE arrangements compliant with the minimum contact wire height and required electrical clearances, considering the allowances and tolerances given in the DART+ Electricity Functional Requirement Specification System-Wide (MAY-MDC-ELE-DART-SP-E-0002).

Sufficient clearance must be achieved at overbridges such that overhead wires can be placed at the correct height for future electrified trains' pantographs, along with provision of necessary allowances for tolerance, adjustment and electrical isolation.

From an OHLE point of view, various equipment arrangements exist and are selected based upon a hierarchy of preference from a systems perspective and the current available bridge clearance. Selection of the electrical case is a purely technical exercise and not subject to a multi-criteria analysis (MCA) process. It is deemed that an electrical-only solution is always the most preferable option wherever this is not a derogation from standards due to insufficient bridge soffit height. Should an electrical-only solution not be possible, other design options are explored - see section 6.2.

This document should be read in conjunction with the other reports which describe the electrification package of work - see Table 1-1.

Table 1-1: List of key documents associated with Electrification of the Northern Line from Malahide to Drogheda

| Annex | Section | Title |
| :---: | :---: | :---: |
| 3.2 | A | OHLE system |
|  | B | OHLE foundation solutions |
|  | C | OHLE support solutions at underbridges |
|  | D | Bridge parapet modifications for OHLE |
|  | E | OHLE Bridge Clearance works |
|  | E1 | OBB39 Option Selection Report |
|  | E2 | OBB44 Option Selection Report |
|  | E3 | OBB55 Option Selection Report |
|  | E4 | OBB78 Option Selection Report |
|  | E5 | OBB80/80A/80B Option Selection Report |
|  | E6 | OBB81 Option Selection Report |
|  | F | Traction Power Supply |
|  | G | User worked level crossing south of Donabate |
|  | H | Fencing and lineside safety |
|  | I | Drogheda Station Canopies |

DART+
Coastal North

## 2. EXISTING SITUATION

### 2.1 Overview

As part of the DART+ Coastal project, the Northern Line between Malahide and Drogheda is to be electrified with 1.5 kV DC overhead line electrification. The OHLE foundation solutions report (Annex
3.2: Section B) provides a general overview of ground conditions. Factors for bridge-specific locations are listed within the relevant sections of this report.

### 2.2 Structures

There are 30 overbridges along the length of track which is to be electrified between Malahide and Drogheda and one additional proposed overbridge is also planned. The existing overbridges are, generally, historic structures and hence were constructed without cognisance of necessary clearances for OHLE.

For an overview of the bridge locations, please refer to Annex 1: Schematic Drawings.
A summary of the criteria relevant to the bridge clearance works is provided in Table 2-1 below. It should be noted that clearances and widths are shown in bold, where confirmed by survey. Other approximate dimensional information has been provided by IÉ. Clearances stated are measured from top of rail (ToR) to bridge soffit.

Table 2-1: Relevant information for clearance works to existing overbridges between Malahide and Drogheda

| Overbridge | Name | Approx. Location |  | Function | Arch | Station | Clearance (ToR - Soffit) ${ }^{(1)}$ <br> (mm) | Approx. Width (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Miles | Yards |  |  |  |  |  |
| OBB32A | DONABATE BYPASS (CLONBURRIS BRIDGE) | 11 | 0 | Road | No | No | $\sim 5800$ | 23.0 |
| OBB32B | PEDESTRIAN CYCLE BRIDGE | - | - | Footbridge | No | No | $\sim 6000$ | 5.6 |
| OBB33 | DONABATE STATION ROADBRIDGE | 11 | 727 | Road | No | Yes | ~5000 | 12.2 |
| OBB33A | DONABATE FOOTBRIDGE | 11 | 784 | Footbridge | No | Yes | $\sim 5100$ | 2.2 |
| OBB35 | BEAVERSTOWN GOLF CLUB | 12 | 445 | Road | No | No | 4740 | 4.5 |
| OBB38 | ROGERSTOWN LANE | 13 | 999 | Road | Yes | No | $\sim 5020$ | 4.6 |
| OBB38A | RUSH \& LUSK FOOTBRIDGE | 13 | 1564 | Footbridge | No | Yes | $\sim 5200$ | 3.0 |
| OBB39 | RUSH \& LUSK ROADBRIDGE | 13 | 1644 | Road | No | Yes | 4775 | 10.7 |
| OBB41 | KINGSTOWN/PUBLIC ROAD | 14 | 438 | Road | No | No | 4700 | 6.9 |
| OBB44 | TYRRELSTOWN/PUBLIC ROAD | 14 | 1437 | Road | No | No | 4585 | 7.4 |


| Overbridge | Name | Approx. Location |  | Function | Arch | Station | Clearance (ToR - Soffit) ${ }^{(1)}$ (mm) | Approx. Width (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Miles | Yards |  |  |  |  |  |
| OBB45 | HJ2DA | 15 | 856 | Road | No | No | 4715 | 4.8 |
| OBB46 | BALDONGAN | 16 | 172 | Road | No | No | $\sim 4860$ | 7.1 |
| OBB47 | SKERRIES GOLF CLUB | 16 | 1038 | Road | Yes | No | 4900 | 5.1 |
| OBB49 | GOLF LINKS RD SKERRIES | 17 | 524 | Road | No | No | 4690 | 8.1 |
| OBB51A | SKERRIES FOOTBRIDGE | 17 | 1708 | Footbridge | No | Yes | 4815 | 2.6 |
| OBB54 | LADIES STAIRS | 19 | 1440 | Footbridge | No | No | $\sim 5100$ | 2.5 |
| OBB55 | COUNTY BRIDGE/PUBLIC ROAD | 21 | 304 | Road | No | No | 4590 | 11.5 |
| OBB57A | BALBRIGGAN FOOTBRIDGE | 21 | 1328 | Footbridge | No | Yes | 4775 | 2.4 |
| OBB62 | FRANKINS/OCCUPATION ROAD | 22 | 1573 | Road | No | No | $\sim 4880$ | 7.9 |
| OBB63 | FILGATE'S/OCCUPATION ROAD | 23 | 866 | Road | No | No | 4735 | 4.9 |
| OBB66 | GORMANSTON STATION ROADBRIDGE | 24 | 19 | Road | No | Yes | 4880 | 4.5 |


| Overbridge | Name | Approx. <br> Location |  | Function | Arch | Station | Clearance (ToR - Soffit) ${ }^{(1)}$ (mm) | Approx. Width (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Miles | Yards |  |  |  |  |  |
| OBB66A (TBC) | GORMANSTON STATION NEW FOOTBRIDGE |  |  |  |  |  | $\sim 5270$ | 2.5 |
| OBB68 | IRISHTOWN/PUBLIC ROAD | 24 | 1757 | Road | No | No | 4920 | 6.6 |
| OBB74A | LAYTOWN FOOTBRIDGE | 27 | 186 | Footbridge | No | Yes | $\sim 5100$ | 2.8 |
| OBB77 | PILTOWN/COLP EAST | 29 | 1452 | Road | No | No | $\sim 4850$ | 8.2 |
| OBB78 | COLPE BRIDGE/PUBLIC ROAD | 30 | 233 | Road | No | No | 4680 | 17.5 |
| OBB80A | MCGRATH'S LANE DROGHEDA | 31 | 758 | Road | Yes | No | 4205 | 6.9 |
| OBB80 | MCGRATH'S LANE DROGHEDA | 31 | 869 | Road | Yes | No | 4300 | 6.6 |
| OBB80B | MCGRATH'S LANE DROGHEDA | 31 | 871 | Road | No | No | 4910 | 7.2 |
| OBB81 | MacBRIDE STATION | 31 | 1259 | Footbridge | No | Yes | 4465 | 2.8 |
| OBB81C | MacBRIDE STATION | 31 | 1262 | Footbridge | No | Yes | 5800 | 4.4 |

NTA
$0|=|$
larrród Eireann lrish Rail

- DART+

Coastal North

DART+
Coastal North

## Notes:

1) Vertical clearance heights were initially based on information received from IÉ, based on field measurements. The heights based on this information include an approximate sign ( $\sim$ ) in front of them in the table. Bridge specific topographical surveys were undertaken on bridges identified as having a low clearance. The results from these surveys are shown in bold.
2) Bridge specific topographical surveys were undertaken on bridges identified as having a low clearance, therefore lateral clearance has been determined from that survey for these bridges. In these cases, pantograph gauge and OHLE wire and supports (where applicable) have been included in the overbridge cross sections obtained from the survey to check the lateral clearance for OHLE wires. For flat overbridges, the lateral clearance is not a limiting factor for the OHLE solution (contact wire and catenary wires) through the bridges, so it is considered that it will also not be a limiting factor for the overbridges which do not have the survey currently available. Furthermore, assessment of installation of parallel feeder wires through the overbridges is being developed. According to the DART+ Electricity Functional Specifications System-Wide document they are preferably installed aerially supported on the OHLE structures. However, when this is not possible because of the available clearance of the overbridge, it will be passed to an isolated cable and clamped to the structure or by any other means or buried.

### 2.3 Permanent Way

Generally, at all overbridge locations there are two tracks which are continuous welded rail on ballast. The exception is at Drogheda Depot and OBB80 at Drogheda Station.

### 2.4 Other Railway Facilities

Seven stations exist along the route to be electrified. These are as follows:

- Donabate: Platforms 1 and 2
- Rush \& Lusk: Platforms 1 and 2
- Skerries: Platforms 1 and 2
- Balbriggan: Platforms 1 and 2
- Gormanston: Platforms 1 and 2
- Laytown: Platforms 1 and 2
- Drogheda MacBride: Platforms 1,2 and 3

Where overbridges are adjacent to or within station platforms, the OHLE wire height needs to be cognisant of the requirements to have increased separation between the public and electrical equipment.

### 2.5 Utilities

There are extensive utility networks in the area surrounding the railway, particularly in the urban areas through which it passes. Service providers with network assets in the area, from whom records have been obtained, include:

- Gas Networks Ireland;
- Irish Water (Water Supply);
- Irish Water (Foul Water Sewers);

DART+
Coastal North

- Dublin City Council (Storm Water Sewers);
- Fingal County Council (Storm Water Sewers);
- ESB Networks - Low, Medium and High Voltage Networks;
- EirGrid
- Eir;
- BT Ireland;
- Irish Rail - Lineside cables parallel to the railway line.

Utility service records have been obtained from all providers in the area. Most services are located within the existing road network surrounding the railway, and in bridge and underpass crossings of the railway. There are also lineside services running parallel to the railway and some major utilities crossing perpendicularly under the railway. All records should be considered indicative only and must be verified prior to any intrusive works occurring.

The records indicate that there are services at track level or within the railway corridor. These include Irish Rail lineside cables, Eir telecoms cables and BT telecoms cables running parallel to the railway from Malahide to Drogheda.

There are several railway overbridges that have utilities located within them. These are as follows:

- OBB33 at Donabate Station contains underground telecommunications.
- OBB39 at Rush \& Lusk Station contains underground telecommunications.
- OBB55 at the R127 road contains underground medium voltage electrical, telecommunications and a 125 mm diameter medium pressure gas main.
- OBB78 at the L1611 road contains underground telecommunications and a 180 mm diameter medium pressure gas main.

DART+
Coastal North

## 3. REQUIREMENTS

The main project requirements relevant to this report subsection are as follows:

- Electrification of the line from the end of the current electrified section at Malahide to Drogheda with 1500V DC overhead;
- Undertake necessary infrastructure change to achieve the clearances required for electrification at bridges and structures;
- Undertake safety improvements resulting from the introduction of 1500 V DC overhead.


### 3.1 Specific Requirements

In achieving the clearances required for electrification at bridges and structures, a predefined approach for electrical clearance design has been adopted as per DART+ Electricity Functional Specifications System-Wide (MAY-MDC-ELE-DART-SP-E-0002) Section 5.6.7. This lists relevant electrical equipment configurations and their hierarchy for adoption and is explained further in section 5.1 of this report.

### 3.2 Systems Infrastructure and Integration

Integration with the signalling system needs to be considered, as well as integration with other electrical cables including OHLE feeder cables though the bridge structure.

### 3.3 Design Standards

Table 3-1 contains the key applicable standards that will be used to develop the design. Please note that this is not intended as an exhaustive list.

Table 3-1: Relevant design standards for OHLE bridge clearance works

| Source | Description | Comments |
| :--- | :--- | :--- |
| European Norm | EN50122-1 | Protective provisions against <br> electric shock |
| European Norm | EN50119 | Electric traction overhead <br> contact lines |
| Irish Rail | I-ETR-4101 | Maintenance Parameters for <br> 1500Vdc OHLE |
| Irish Rail | CCE-TMS-300 | Track Construction <br> Requirements and Tolerances |
| Irish Rail | CME-TMS-306 | OHLE Interface for IÉ Rolling <br> Stock |



- larnrōd Éireann lrish Rail $\quad$ ITD

DART+
Coastal North

| Source | Description | Comments |
| :--- | :--- | :--- |
| Irish Rail | CCE-TMS-321 | Track Maintenance <br> Requirements and Tolerances |
| Irish Rail | CME-TMS-327 | Vehicle gauging |
| Irish Rail | CCE-TMS-410 | Civil Engineering Structures <br> Design Standard |
| Irish Rail | I-PWY-1101 | Requirements for Track and <br> Structures Clearances |
| Irish Rail | SET-AMS-002-012 Iss1.0 | Derogation from SET <br> Technical Standards |

DART+
Coastal North

## 4. CONSTRAINTS

### 4.1 Technical

### 4.1.1 Electrical system

- The total clear height required at any bridge is a sum of the following:
- The desired contact wire height;
- The track maintenance tamping allowance;
- The track construction tolerance;
- The track maintenance tolerance;
- The OHLE construction tolerance;
- The OHLE maintenance tolerance;
- The structural construction tolerance if bridge reconstruction/modification is required;
- An allowance for contact wire and pantograph wear;
- The OHLE system height or allowance for OHLE support;
- The uplift caused to wires by a passing train;
- The required electrical clearances;
- The survey tolerance.


### 4.1.1.1 Contact wire height

The height of the contact wire (from which the train pantograph draws its power) is defined by system requirements as having a target height of 4.7 m . A number of electrical equipment arrangements exist to achieve this, each compatible with differing bridge soffit heights. This can also be reduced to a height of 4.4 m before a derogation from standards is required, with a risk assessment and approval from IÉ SET (and CCE depending on values for allowances, tolerances and clearances). The absolute minimum is 4.27 m .

In case of modifications of overbridges or construction of new overbridges, passive provision for 25 kV a.c. electrification will be considered. In this case, the minimum nominal contact wire height should be 5 m instead of 4.7 m as per section 5.24 .2 of the DART+ Program Electricity FRS MAY-MDC-ELE-DART-SP-E-0002, in order to fulfil with the TSI requirements.

However, according to the TSI (table 4.2.9.1.) the minimum design contact wire height can be lower in accordance with EN 50119 clause 5.10.5 depending on the chosen gauge.

| Contact wire height |  |  |
| :---: | :---: | :---: |
| Description | $\mathrm{v} \geq 250[\mathrm{~km} / \mathrm{h}]$ | v < 250 [ $\mathrm{km} / \mathrm{h}]$ |
| Nominal contact wire height [mm] | Between 5080 and 5300 | Between 5000 and 5750 |
| Minimum design contact wire height [ mm ] | 5080 | In accordance with EN 50119:2009, clause 5.10.5 depending on the chosen gauge |
| Maximum design contact wire height [mm] | 5300 | $6200{ }^{(1)}$ |
| ${ }^{(1)}$ Taking into account tolerances and uplift in accordance with EN 50119:2009 figure 1, the maximum contact wire height shall not be greater than 6500 mm . |  |  |

Figure 4-1: Table 4.2.9.1. of the Energy Subsystem TSI
Clause 5.10.4.3 of EN 50119 states that the minimum design contact wire height shall be calculated by adding all downwards movements of the contact wire to the minimum height. The minimum contact wire height is calculated by adding the electrical clearance to the swept envelope height of the rolling stock. Consideration is therefore given to:

- Vehicle gauge (IRL2 CME-TMS-327): 4064 mm
- Electrical clearance: 270/150 mm (Static/Passing)
- Vertical tolerance on the track position: TMTA 100/75/50 mm
- Downwards installation tolerance for the contact wire: 50 mm (Construction plus maintenance tolerances as per section 5.6.6. FRS)
- Downwards dynamic movements of the contact wire: $0 / 110 \mathrm{~mm}$
- Effects of ice load and temperature on the conductors: Depending on the span as per values given by Appendix K of the FRS.


### 4.1.1.2 Track maintenance tamping allowance

Track tamping is the regular maintenance process of correcting geometry and creating a uniform rail bed via adjustments to the ballast. This is generally achieved by a rail-mounted tamping machine. The target maintenance allowance is 100 mm although this can be reduced to a minimum of 50 mm for ballasted track. Alternatively, the rails can be mounted directly to a concrete slab (referred to as slab track) to remove the need for tamping (i.e. Omm allowance).

### 4.1.1.3 Track maintenance tolerance

Track Maintenance Tolerance of 25 mm for ballast track is considered in the required clear height.

### 4.1.1.4 Track and OHLE construction tolerance

Track and OHLE construction tolerances are 5 mm and 20 mm respectively.

### 4.1.1.5 OHLE maintenance tolerance

During the service lifetime of the OHLE, maintenance operations and adjustments require a tolerance of 30 mm , regardless of electrical arrangement selected.

### 4.1.1.6 Contact wire and pantograph wear

An allowance of 25 mm is required to account for wear to the pantograph and contact wire affecting the dynamic behaviour of the system.

### 4.1.1.7 System height

The system height is the distance between the highest point of the catenary wire within the area underneath the bridge soffit and the contact wire. Typically, support is provided to the contact wire from the catenary wire with 'droppers' as shown in Figure 4-2. The dropper heights can vary from 500 to 100 mm .

It is possible to place the catenary and contact wires at the same height and hence reduce the system height to 0 mm . This is referred to as a contenary system and is shown in Figure 4-3. This

DART+
Coastal North
system requires reduced support spacing such that the tension in the contact wire is enough to keep it sufficiently level. This is a maximum distance of $12-13 \mathrm{~m}$. Since OHLE masts must be a minimum of 2 m from the bridge structure, if the bridge deck is wider than 8 m then intermediate support arms fixed to the soffit are required. This is referred to as a 'fitted' system, the preferable opposite of which is a 'free running' system.


Figure 4-2: Example of typical catenary support to contact wire with 500 mm droppers, passing under example bridge


Figure 4-3: Example of typical contenary support showing achievement of a system height of 0 mm underneath a reduced clearance bridge

In case of fitted solution, an allowance of 120 mm is considered for the installation of the OHLE support arms.

### 4.1.1.8 Uplift

Passing trains cause movement on the overhead wires. This is relevant when considering dynamic electrical clearance required. For a catenary system, the required dynamic uplift allowance is 110 mm . For a contenary system this is typically 70 mm but may be reduced to 50 mm at reduced clearance overbridges.

### 4.1.1.9 Electrical clearance

Enhanced electrical clearance (the preferred option) is 150 mm under static conditions or 100 mm under dynamic for 1.5 kV d.c. Note that the dynamic case governs as this requires the inclusion of uplift allowance. Reduced electrical clearances are 100 mm and 80 mm under static and dynamic conditions respectively.

In case of modifications of overbridges or construction of new overbridges, passive provision for 25 kV a.c. electrification will be considered, so in this case, electrical clearances are 270 mm and 150 mm under static and dynamic conditions respectively.

DART+
Coastal North

### 4.1.1.10 Surveying

An allowance of 5 mm for survey inaccuracies is required.

### 4.1.2 Gauging

The necessary changes to electric rolling stock on this section of the route requires consideration of gauging (physical clearances) as well as the previously discussed electrical clearances. This is particularly relevant to the pantograph and its interaction with arched bridge profiles. As shown in Figure 4-4 below, this may constrain the track alignment within the bridge cross section and impact on the proposed solution.


Figure 4-4: Example of pantographs clashing with bridge soffit

### 4.1.3 Track Level

Track lowering is an option to improve the bridge soffit height and enable a more favourable electrical arrangement. Track lowering can be achieved in two ways:

- Removal of some of the ballast depth - skim dig;
- Adjustment of formation level.

A skim dig can be achieved in some conditions by temporarily supporting rails and digging out some of the ballast from underneath sleepers. This is a relatively simple task with limited construction impact but can only achieve minor reductions to track levels (less than $\sim 75 \mathrm{~mm}$ ).

For lowering greater than 75 mm , the potential construction operations will be more disruptive. Where enough ballast depth exists, this may be possible via alterations to the overall ballast depth. In cases with minimal ballast depth, the formation may need to be lowered, comprising significantly disruptive construction activities, including removal of track and ballast before the formation can be dug down, followed by reinstatement. It should be noted that further investigation into the existing ballast depth at such locations will be required at subsequent design stages.

Due to gradient limits and vertical curve requirements on track alignment, any lowering operation is likely to impact extensive lengths of rail. Consideration must be given to the interaction with other assets such as station platforms.

DART+
Coastal North

Lowering of track is also constrained by impacts on existing drainage, utilities and bridge substructure.

### 4.1.4 Bridge Modification

As an alternative to track lowering, bridge modification can be considered to achieve additional vertical clearance where alternative solutions prove too constrictive. This can either take the form of raising the bridge superstructure or adopting a more substantial modification/reconstruction of the bridge to achieve the required clearance.

Raising the superstructure is typically achieved by either demolishing and reconstructing the superstructure or jacking up the existing bridge beams and resetting the deck at a higher level. Adjustment to the road level above and tie-in with the road alignment is required. This has a direct impact on the road geometry, particularly the vertical alignment. Many bridges over the existing line have already been raised with noticeably pronounced vertical crest curves and poor intervisibility. Any services carried by the deck above would need to be temporarily diverted or disconnected as part of the works. The existing bridge would need to be structurally assessed to ensure it is suitable for the altered configuration. This type of solution would retain the existing lateral clearance to the abutments.

Similarly, bridge reconstruction would require the structure to be taken out of commission for the duration of the build, while new foundations, abutment walls and deck are constructed. Where a full bridge reconstruction is proposed, it would need to meet the vertical and lateral clearance requirements of the relevant standards (CCE-TMS-410 in particular must be complied to among other standards), considering a passive provision for 25 kV a.c. electrification. Where this cannot be achieved, a derogation will be required.

Unless the works can be done offline, any bridge modification option would have an impact on accessibility and would rely on a suitable alternative route to be put in place during construction.

### 4.2 Environmental

For a more detailed overview of the existing environmental constraints for DART+ Coastal North refer to Annex 3.1 Constraints Report and the individual option selection reports that can be found in Annexes E1 to E6.

DART+
Coastal North

## 5. ELECTRICAL SOLUTION ASSESSMENT

This section reviews whether electrical solutions are possible at each bridge location. The minimum vertical clearance is checked at each bridge and a best fit electrical solution applied based on the hierarchies outlined in the project specification.

### 5.1 Electrical Case Hierarchy

As detailed in section 4.1, a variety of electrical arrangements exist to cater for different available clearances. These are given a hierarchy of preference as shown in Table 5-1. This is as provided and detailed further in section 5.6.7 of the Electricity Functional Specifications System-Wide document (MAY-MDC-ELE-DART-SP-E-0002).

A nominal contact wire height of at least 4700 mm is preferred at overbridge locations. Where this cannot be achieved, a minimum contact wire height (CWH) of 4400 mm can be considered provided the associated risks are suitably addressed. Contact wire heights less than 4400 mm will require a derogation. This is summarised as follows:

- Contact wire height $\geq \mathbf{4 7 0 0} \mathbf{~ m m}$ :

Represents nominal contact wire height. No risk assessment or derogation required. These are coloured green in the table below.

- Contact wire height < $\mathbf{4 7 0 0} \mathbf{~ m m}$ but $\geq \mathbf{4 4 0 0} \mathbf{~ m m}$ :

Electrical solutions with contact wire heights in this range require a risk assessment to be undertaken. These are coloured yellow in the table below.

- Contact wire height < $\mathbf{4 4 0 0} \mathbf{~ m m}$ but > $\mathbf{4 2 0 0} \mathbf{~ m m}$ :

Electrical solutions with contact wire heights less than 4400 mm require a risk assessment and a derogation. These are coloured orange in the table below.

The electrical solution given in the specification favours the contact wire height over the system height. Where possible, the contact wire height is increased, resulting in contenary systems being favoured since increasing the system height typically requires more clearance than that required to increase the system height to a more favourable hierarchy case.

As stated in section 2.2, it should be noted that soffit heights are shown in bold, where confirmed by survey. Other approximate dimensional information has been provided by IÉ.
larnrōd Éireann
lrish Rail

## ARUP

DART+
Coastal North

Table 5-1: Electrical case hierarchy at overbridge structures

|  |  |  |  |  |  |  |  | CW and panto wear |  | $\frac{5}{\frac{5}{2}}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Case 1 <br> CWH of 4700 mm , nominal SH of 1300 mm , current carrying dropper of 500 mm and enhanced EC. | Static EC | 4700 | 100 | 5 | 25 | 20 | 30 | 0 | 500 | 0 | 150 | 5 | 5535 |
|  | Dynamic EC | 4700 | 100 | 5 | 25 | 20 | 30 | 25 | 500 | 110 | 100 | 5 | 5620 |
| Case 2 <br> CWH of 4700 mm , reduced SH with reduced current carrying dropper of 300 mm and enhanced EC. | Static EC | 4700 | 100 | 5 | 25 | 20 | 30 | 0 | 300 | 0 | 150 | 5 | 5335 |
|  | Dynamic EC | 4700 | 100 | 5 | 25 | 20 | 30 | 25 | 300 | 110 | 100 | 5 | 5420 |
| Case 3 <br> CWH of 4700 mm , reduced SH with reduced current carrying dropper of 100 mm and enhanced EC. | Static EC | 4700 | 100 | 5 | 25 | 20 | 30 | 0 | 100 | 0 | 150 | 5 | 5135 |
|  | Dynamic EC | 4700 | 100 | 5 | 25 | 20 | 30 | 25 | 100 | 110 | 100 | 5 | 5220 |
| Case 4 <br> CWH of 4700 mm , reduced SH to zero, contenary and enhanced EC. Uplift 70 mm | Static EC | 4700 | 100 | 5 | 25 | 20 | 30 | 0 | 0 | 0 | 150 | 5 | 5035 |
|  | Dynamic EC | 4700 | 100 | 5 | 25 | 20 | 30 | 25 | 0 | 70 | 100 | 5 | 5080 |
| Case 5 <br> CWH of 4600 mm , reduced SH with reduced current carrying dropper of 300 mm , reduced tamping allowance to 75 mm and enhanced EC. | Static EC | 4600 | 75 | 5 | 25 | 20 | 30 | 0 | 300 | 0 | 150 | 5 | 5210 |
|  | Dynamic EC | 4600 | 75 | 5 | 25 | 20 | 30 | 25 | 300 | 110 | 100 | 5 | 5295 |
| Case 6 | Static EC | 4600 | 75 | 5 | 25 | 20 | 30 | 0 | 100 | 0 | 150 | 5 | 5010 |


|  |  |  |  |  |  |  |  | CW and panto wear |  | $\frac{5}{\frac{5}{0}}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CWH of 4600 mm , reduced SH with reduced current carrying dropper of 100 mm , reduced tamping allowance to 75 mm and enhanced EC. | Dynamic EC | 4600 | 75 | 5 | 25 | 20 | 30 | 25 | 100 | 110 | 100 | 5 | 5095 |
| Case 7 <br> CWH of 4600 mm , reduced SH to zero, contenary, reduced tamping allowance to 75 mm and enhanced EC. Uplift 70 mm | Static EC | 4600 | 75 | 5 | 25 | 20 | 30 | 0 | 0 | 0 | 150 | 5 | 4910 |
|  | Dynamic EC | 4600 | 75 | 5 | 25 | 20 | 30 | 25 | 0 | 70 | 100 | 5 | 4955 |
| Case 8 <br> CWH of 4500 mm , reduced SH with reduced current carrying dropper of 300 mm , reduced tamping allowance to 50 mm and enhanced EC. | Static EC | 4500 | 50 | 5 | 25 | 20 | 30 | 0 | 300 | 0 | 150 | 5 | 5085 |
|  | Dynamic EC | 4500 | 50 | 5 | 25 | 20 | 30 | 25 | 300 | 110 | 100 | 5 | 5170 |
| Case 9 <br> CWH of 4500 mm , reduced SH with reduced current carrying dropper of 100 mm , reduced tamping allowance to 50 mm and enhanced EC. | Static EC | 4500 | 50 | 5 | 25 | 20 | 30 | 0 | 100 | 0 | 150 | 5 | 4885 |
|  | Dynamic EC | 4500 | 50 | 5 | 25 | 20 | 30 | 25 | 100 | 110 | 100 | 5 | 4970 |
| Case 10 <br> CWH of 4500 mm , reduced SH to zero, contenary, reduced tamping allowance to 50 mm and enhanced EC. Uplift 70 mm | Static EC | 4500 | 50 | 5 | 25 | 20 | 30 | 0 | 0 | 0 | 150 | 5 | 4785 |
|  | Dynamic EC | 4500 | 50 | 5 | 25 | 20 | 30 | 25 | 0 | 70 | 100 | 5 | 4830 |
| Case 11 <br> CWH of 4400 mm , reduced SH with reduced current carrying dropper of 300 mm , reduced tamping allowance to 50 mm and enhanced EC. | Static EC | 4400 | 50 | 5 | 25 | 20 | 30 | 0 | 300 | 0 | 150 | 5 | 4985 |
|  | Dynamic EC | 4400 | 50 | 5 | 25 | 20 | 30 | 25 | 300 | 110 | 100 | 5 | 5070 |
| Case 12 | Static EC | 4400 | 50 | 5 | 25 | 20 | 30 | 0 | 100 | 0 | 150 | 5 | 4785 |

$$
\text { NTA } \quad \emptyset|=|=10
$$

larnród Éreann
${ }^{1}$ lirishrod Rail

ARUP
DART+
Coastal North

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dynamic EC | 4400 | 50 | 5 | 25 | 20 | 30 | 25 | 100 | 110 | 100 | 5 | 4870 |
| Static EC | 4400 | 50 | 5 | 25 | 20 | 30 | 0 | 0 | 0 | 100 | 5 | 4635 |
| Dynamic EC | 4400 | 50 | 5 | 25 | 20 | 30 | 25 | 0 | 70 | 80 | 5 | 4710 |
| Static EC | 4350 | 50 | 5 | 25 | 20 | 30 | 0 | 0 | 0 | 100 | 5 | 4585 |
| Dynamic EC | 4350 | 50 | 5 | 25 | 20 | 30 | 25 | 0 | 50 | 80 | 5 | 4640 |
| Static EC | 4270 | 0 | 5 | 5 | 20 | 30 | 0 | 0 | 0 | 100 | 5 | 4435 |
| Dynamic EC | 4270 | 0 | 5 | 5 | 20 | 30 | 25 | 0 | 50 | 80 | 5 | 4490 |

### 5.1.1 Risk Assessments

For bridges where a contact wire height of less than 4.7 m is proposed, a risk assessment must be carried out and presented to the IÉ Signalling, Electrification and Telecoms (SET) department. Site specific risks will be evaluated in subsequent design stages however, general risks associated with reduced contact wire heights have been captured.

The figures provided in this section are example extracts from the hazard log and are provided for reference only. ' $F$ ' represents the frequency of the hazard event occurring and ' $C$ ' the consequence.

### 5.1.1.1 General risks

The two risks shown in Figure 51 are associated with all overbridges where the proposed contact wire height is less than 4.7 m . The mitigation measures listed are proposed for each overbridge.


Figure 5-1: General hazards associated with reduced contact wire heights at overbridges

### 5.1.1.2 Station risks

Where an overbridge with reduced contact wire height exists within a station, this introduces further risk as detailed in Figure 52.


Figure 5-2: Hazards within stations associated with reduced contact wire heights at overbridges

### 5.1.1.3 Public use of legacy overbridges and structures with reduced clearances

Similarly, where an overbridge designated for public use has a reduced contact, this introduces further risk as detailed in Figure 53.

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event Description of the Hazard Event (the RISK) and the consequence. | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overrightarrow{y y}} \\ & \stackrel{y}{c} \end{aligned}$ | Safety Measures - mitigation description | F | C | 駡 |
| Restricted electrical clearances of new OHLE at legacy structures, due to local route constraints. | Public use of legacy overbridges and structures with reduced electrical clearances. | Touch potential, Electrocution | 4 | 4 | 8 | Proposed OHLE solution considers static electrical clearance of 100 mm and dynamic electrical clearance of 80 mm , which are the minimum values according to I-ETR4101 / Maintenance Parameters for 1500 Vdc OHLE; chapter 2.2 <br> Electrical Clearances - subchapter 2.2.1 and FRS. | 2 | 4 | 6 |

Figure 5-3: Hazards associated with reduced contact wire heights at overbridges designated for public use

### 5.2 Classification of Bridge Electrical Solutions

The available vertical clearance at each bridge was assessed and an electrical solution proposed based on the requirements of the Functional Specification. Where the soffit of the bridge varies across the width of the tracks (e.g. arch bridges), the pantograph and electrical clearance envelopes were plotted in elevation to confirm proposed solutions.

The electrical solution also takes into account the extra depth needed to install a bridge-arm connection in the case of fitted systems.

Table 5-2 below summarises the proposed electrical solutions at each overbridge location. As for previous tables, bold clearances are those confirmed by survey.

Table 5-2: Summary of the proposed electrical solutions at each overbridge

Irish Rail
ARUP
DART+
Coastal North

| Bridge No. | Soffit <br> Form | $\begin{aligned} & \text { Clearance } \\ & \text { (ToR - Soffit) } \\ & \text { (mm) } \end{aligned}$ | Approx. Abut. Width (m) | Fitted (F) / Free-Running (FR) System | $\begin{aligned} & \text { Proposed } \\ & \text { CWH } \\ & (\mathrm{mm}) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| OBB32A | Flat | $\sim 5800$ | 23.0 | FR | 4700 |
| OBB32B | Flat | $\sim 6000$ | 5.6 | FR | 4700 |
| OBB33 | Flat | ~5000 | 12.2 | F | 4550 |
| OBB33A | Flat | $\sim 5100$ | 2.2 | FR | 4600 |
| OBB35 | Flat | 4740 | 4.5 | FR | 4400 |
| OBB38 | Arch | ~5020 | 4.6 | FR | 4480 |
| OBB38A | Flat | $\sim 5200$ | 3.0 | FR | 4420 |
| OBB39 | Flat | 4775 | 10.7 | F | 4370 |
| OBB41 | Flat | 4700 | 6.9 | FR | 4400 |
| OBB44 | Flat | 4585 | 7.4 | FR | 4320 |
| OBB45 | Flat | 4715 | 4.8 | FR | 4400 |
| OBB46 | Flat | $\sim 4860$ | 7.1 | FR | 4500 |
| OBB47 | Arch | 4900 | 5.1 | FR | 4500 |
| OBB49 | Flat | 4690 | 8.1 | FR | 4400 |
| OBB51A | Flat | 4815 | 2.6 | FR | 4480 |
| OBB54 | Flat | $\sim 5100$ | 2.5 | FR | 4700 |
| OBB55 | Flat | 4590 | 11.5 | F | 4270 |
| OBB57A | Flat | 4775 | 2.4 | FR | 4440 |
| OBB62 | Flat | $\sim 4880$ | 7.9 | FR | 4500 |
| OBB63 | Flat | 4735 | 4.9 | FR | 4400 |

ARUP
DART+
Coastal North

| Bridge No. | Soffit Form | $\begin{aligned} & \text { Clearance } \\ & \text { (ToR - Soffit) } \\ & (\mathrm{mm}) \end{aligned}$ | Approx. Abut. Width (m) | Fitted (F) Free-Running (FR) System | Proposed CWH (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| OBB66 | Flat | 4880 | 4.5 | FR | 4525 |
| TBC | Flat | $\sim 5270$ | 2.5 | FR | 4645 |
| OBB68 | Flat | 4920 | 6.6 | FR | 4540 |
| OBB74A | Flat | $\sim 5100$ | 2.8 | FR | 4700 |
| OBB77 | Flat | $\sim 4850$ | 8.2 | F | 4400 |
| OBB78 | Flat | 4680 | 17.5 | F | 4290 |
| OBB80 | Arch | 4205 | 6.9 | - | - |
| OBB80A | Arch | 4300 | 6.6 | - | - |
| OBB80B | Flat | 4910 | 7.2 | FR | 4530 |
| OBB81 | Flat | 4465 | 2.8 | FR | 4270 |
| OBB81C | Flat | 5800 | 4.4 | FR | 4700 |

The table above uses various shades of colour to differentiate between the various electrical solutions proposed. These are as follows:

- Green indicates solutions with a nominal contact wire height (CWH $\geq 4700 \mathrm{MM}$ ) ;
- Yellow indicates solutions which require a risk assessment ( $4700 \mathrm{~mm}<\mathrm{CWH} \leq 4400 \mathrm{MM}$ );
- Blue indicates solutions which would require a derogation and risk assessment (CWH < 4400 mm ). These are potential solutions only, refer to section 5.3 for details);
- Orange indicates that no electrical solution is possible at this location.


### 5.2.1 Electrical solutions adopting a Nominal Contact Wire Height ( 4700 mm )

The bridges listed in the table below have sufficient vertical clearance to adopt an electrical solution with a contract wire height of 4700 mm .

Table 5-3: Bridges with a proposed contact wire height of 4700 mm

| Bridge No. | Clearance <br> $($ ToR - Soffit $)$ <br> $(\mathrm{mm})$ | Proposed <br> CWH <br> $(\mathrm{mm})$ | Comment |
| :---: | :---: | :---: | :--- |
| OBB32A | $\sim 5800$ | 4700 | Road bridge recently constructed as part of the <br> Donabate relief road. |

DART+
Coastal North

| OBB32B | $\sim 6000$ | 4700 | Proposed future pedestrian cycle bridge at <br> south of Donabate station |
| :---: | :---: | :---: | :--- |
| OBB54 | $\sim 5100$ | 4700 | Ladies Stairs pedestrian bridge. <br> Bridge arms installed on dedicated OHLE <br> structures each side of the signals on the <br> southern side |
| OBB74A | $\sim 5100$ | 4700 | Pedestrian bridge at Laytown Station. <br> Bridge arms installed on dedicated OHLE <br> structures each side of bridge in platform area. |
| OBB81C | 5800 | 4700 | Relatively new footbridge at Drogheda <br> MacBride Station used by maintenance staff to <br> access the depot building. |

Please note that distance between the uplifted pantograph and the overbridge soffit for OBB54 and OBB74A is 125 mm .

### 5.2.2 Electrical Solutions requiring a risk assessment

The proposed electrical solution for bridges where the contact wire height is less than 4700 mm but greater than or equal to 4400 mm is summarised the tables below. A risk assessment has been undertaken for the solutions at each of these bridges and is contained in Appendix A of this report.

Iarnród Éireann
Irish Rail
ARUP
DART+
Coastal North

Table 5-4: Proposed electrical solution with $4500 \mathrm{~mm} \leq$ CWH $<4700 \mathrm{~mm}$

|  | OBB33 | OBB33A | OBB46 | OBB47 | OBB62 | OBB66 | OBB66A <br> (TBC) | OBB68 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Current Structure Parameters |  |  |  |  |  |  |  |  |
| Structure Name | Donabate Station Roadbridge | Donabate Station Footbridge | Baldongan | Skerries Golf Club | Frankins/Occu pation Road | Gomrnaston Station Roadbridge | Gormanston St. Footbridge (planned) | Irishtown/Publi c Road |
| Chainage | $\begin{gathered} 11 \text { miles \& } 727 \\ \text { yards } \end{gathered}$ | $\begin{gathered} 11 \text { miles \& } 784 \\ \text { yards } \end{gathered}$ | $\begin{aligned} & 16 \text { miles \& } 172 \\ & \text { yards } \end{aligned}$ | 16 miles \& 1038 yards | 22 miles \& 1573 yards | 24 miles \& 19 yards | $\begin{aligned} & 24 \text { miles \& } 120 \\ & \text { yards } \end{aligned}$ | 24 miles \& 1757 yards |
| Bridge Type | Roadbridge | Footbridge | Roadbridge | Roadbridge | Roadbridge | Roadbridge | Footbridge | Roadbridge |
| Is the Structure Listed | Yes | No | No | No | No | No | No | No |
| Width of Structure | 12.2 | 2.2 | 7.1 | 4.7 | 7.9 | 4.5 | 2.6 | 6.6 |
| Worst Vertical Clearance <br> - TOR to Soffit | ~5000 | $\sim 5100$ | $\sim 4860$ | 4900 | $\sim 4880$ | 4880 | $\sim 5274$ | 4920 |
| Structure type | Flat | Flat | Flat | Arched | Flat | Flat | Flat | Flat |
| Bridge Constraints | Donabate station | Donabate station, OBB33 | None | None | None | Gormanston station, New footbridge | Gormanston station, OBB66 | None |
| Proposed OHLE solution | Contenary with zero encumbrance | OHLE with minimum dropper of 100 mm | Contenary with zero encumbrance | OHLE with minimum dropper of 100 mm | Contenary with zero encumbrance | Contenary with zero encumbrance | OHLE with minimum dropper of 100 mm | Contenary with zero encumbrance |

Table 5-5: Proposed electrical solution parameters with $4500 \mathrm{~mm} \leq \mathrm{CWH}$ < 4700 mm

|  | OBB33 | OBB33A | OBB46 | OBB47 | OBB62 | OBB66 | OBB66A <br> (TBC) | OBB68 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Proposed OHLE solution | Contenary with zero encumbrance | OHLE solution with minimum dropper of 100 mm | Contenary with zero encumbrance | OHLE solution with minimum dropper of 100 mm | Contenary with zero encumbrance | Contenary with zero encumbrance | OHLE solution with minimum dropper of 100 mm | Contenary with zero encumbrance |
| OHLE Arrangement | Fitted with Elastic Bridge Arms | Free Running | Free Running | Free Running | Free Running | Free Running | Free Running | Free Running |
| Static Clearance (Csc) 1500 Vdc | 150 | 150 | 150 | 150 | 150 | 150 | 270 | 150 |
| Dynamic Clearance (Cdc) 1500 Vdc | 100 | 100 | 100 | 100 | 100 | 100 | 150 | 100 |
| Minimum Position of the Contact Wire (considering tamping) | 4411 | 4352 | 4336 | 4223 | 4311 | 4361 | 4421 | 4351 |
| Actual Design Contact Wire Height (Cdcl) (After Tamping) | 4550 | 4600 | 4500 | 4500 | 4500 | 4525 | 4645 | 4540 |
| Maximum Design Contact Wire Height [Pre-Tamping] | 4600 | 4675 | 4575 | 4575 | 4600 | 4600 | 4745 | 4640 |
| OHLE System Depth (Csd) | 0 | 110 | 0 | 0 | 0 | 0 | 150 | 0 |

larnrod Eireann Irish Rail

ARUP
DART+
Coastal North

|  | OBB33 | OBB33A | OBB46 | OBB47 | OBB62 | OBB66 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (TBC) |  |  |  |  |  |  |

NTA $\quad \square$
larnród Eireann lrish Rail
Irish Rail

ARUP

Coastal North

|  | OBB33 | OBB33A | OBB46 | OBB47 | OBB62 | OBB66 | OBB66A <br> (TBC) | OBB68 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Acceptance - CCE | TMTA 50 mm | TMTA 75 mm | TMTA 75 mm <br> Mech. <br> clearance 110 mm | TMTA 75 mm <br> Mech. <br> clearance 110 mm | $\begin{aligned} & \text { Mech. } \\ & \text { clearance } 105 \\ & \mathrm{~mm} \end{aligned}$ | TMTA 75 mm <br> Mech. <br> clearance 105 mm | No | Mech. <br> clearance 105 mm |
| Acceptance - SET | CW<4700 mm | CW<4700 mm | CW<4700 mm | CW<4700 mm | CW<4700 mm | CW<4700 mm | CW<4700 mm | CW<4700 mm |
| Derogation - SET | No | No | No | No | No | No | No | No |

larnrōd Éireann
Irish Rail
ARUP
DART+
Coastal North

Table 5-6: Proposed electrical solution with $4400 \leq \mathrm{CWH}<4500 \mathrm{~mm}$

|  | OBB35 | OBB38 | OBB38A | OBB41 | OBB49 | OBB51A | OBB57A | OBB63 | OBB77 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Current Structure Parameters |  |  |  |  |  |  |  |  |  |
| Structure Name | Beaverstown Golf Club | Rogerstown Lane | Rush \& Lusk Footbridge | Kingstown/ <br> Public Road | Golf Links <br> Road <br> Skerries | Skerries <br> Footbridge | Balbriggan Footbridge | Filgate's/ Occupation Road | Piltown |
| Chainage | 12 miles \& 445 yards | 13 miles \& 999 yards | 13 miles \& 1564 yards | 14 miles \& 438 yards | 17 miles \& 524 yards | 17 miles \& 1708 yards | 21 miles \& 1328 yards | 23 miles \& 866 yards |  <br> 1452 yards |
| Bridge Type | Roadbridge | Roadbridge | Footbridge | Roadbridge | Roadbridge | Footbridge | Footbridge | Roadbridge | Roadbridge |
| Is the Structure Listed | No | No | No | No | No | No (but located in a station which protected) | No (but located in a station which protected) | No | No |
| Width of Structure | 4.5 | 4.6 | 3.0 | 6.7 | 7.4 | 2.3 | 2.4 | 4.5 | 8.2 |
| Worst Vertical Clearance - TOR to Soffit | 4740 | $\sim 5020$ | $\sim 5200$ | 4703 | 4690 | 4815 | 4775 | 4735 | $\sim 4850$ |
| Structure type | Flat | Arched | Flat | Flat | Flat | Flat | Flat | Flat | Flat |
| Bridge Constraints | - | - | Rush \& Lusk station, OBB39 | - |  | Skerries station | Balbriggan station |  |  |
| Proposed OHLE solution | Contenary with zero encumbranc e | Contenary with zero encumbranc e | OHLE with minimum dropper of 300 mm | Contenary with zero encumbranc e | Contenary with zero encumbranc e | Contenary with zero encumbranc e | Contenary with zero encumbranc e | Contenary with zero encumbranc e | Contenary with zero encumbranc e |

Table 5-7: Proposed electrical solution parameters with $4400 \leq \mathrm{CWH}<4500 \mathrm{~mm}$

|  | OBB35 | OBB38 | OBB38A | OBB41 | OBB49 | OBB51A | OBB57A | OBB63 | OBB77 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Proposed OHLE solution | Contenary with zero encumbrance | Contenary with zero encumbrance | OHLE <br> solution with minimum dropper of 300 mm | Contenary with zero encumbrance | Contenary <br> with zero encumbrance | Contenary with zero encumbrance | Contenary with zero encumbrance | Contenary with zero encumbrance | Contenary with zero encumbrance |
| OHLE Arrangement | Free Running | Free Running | Free Running | Free Running | Free Running | Free Running | Free Running | Free Running | Fitted with Elastic Bridge Arms |
| Static Clearance (Csc) 1500 Vdc | 100 | 100 | 150 | 100 | 100 | 100 | 100 | 100 | 100 |
| Dynamic Clearance (Cdc) <br> - 1500 Vdc | 80 | 80 | 100 | 80 | 80 | 80 | 80 | 80 | 80 |
| Minimum Position of the Contact Wire (considering tamping) | 4236 | 4316 | 4221 | 4275 | 4275 | 4316 | 4276 | 4236 | 4261 |
| Actual Design Contact Wire Height (Cdcl) (After Tamping) | 4400 | 4480 | 4420 | 4400 | 4400 | 4480 | 4440 | 4400 | 4400 |
| Maximum Design Contact Wire Height [PreTamping] | 4475 | 4555 | 4495 | 4450 | 4450 | 4555 | 4515 | 4475 | 4450 |
| OHLE System Depth (Csd) | 0 | 0 | 320 | 0 | 0 | 0 | 0 | 0 | 0 |

larrród Éireann lirish Rail

ARUP
DART+
Coastal North

|  | OBB35 | OBB38 | OBB38A | OBB41 | OBB49 | OBB51A | OBB57A | OBB63 | OBB77 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OHLE Uplift (Cwu) | 70 | 70 | 110 | 50 | 50 | 70 | 70 | 70 | 70 |
| OHLE Construction/ Installation (Cct) + Maintenance Tolerance (Cmt) | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 |
| Structure Construction Tolerance (St) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Track Maintenance <br> Tamping Allowance (Tla) | 75 | 75 | 75 | 50 | 50 | 75 | 75 | 75 | 50 |
| Track Construction Tolerance (Tct) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Track Maintenance Tolerance (Tmt) | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 |
| Considered OHLE span through the overbridge (as per hierarchy cases) | 15 | 15 | 30 | 12 | 12 | 15 | 15 | 15 | 15 |
| Sag and lce Load | 39 | 39 | 74 | 25 | 25 | 39 | 39 | 39 | 39 |
| Survey Tolerance | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Loading Gauge | 4064 | 4064 | 4064 | 4064 | 4064 | 4064 | 4064 | 4064 | 4064 |
| Mechanical Clearance | 90 | 290 | 490 | 98 | 85 | 85 | 85 | 85 | 225 |
| Speed through the structure | $160 \mathrm{~km} / \mathrm{h}$ 100 mph | 160km/h 100 mph | 160km/h 100 mph | 160km/h 100 mph | 160km/h 100 mph | 160km/h 100 mph | 160km/h 100 mph | 160km/h 100 mph | 160km/h 100 mph |



DART+
Coastal North

|  | OBB35 | OBB38 | OBB38A | OBB41 | OBB49 | OBB51A | OBB57A | OBB63 | OBB77 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Acceptance - CCE | TMTA 75 mm <br> Mech. clearance 90 mm | TMTA 75 mm | TMTA 75 mm | TMTA 50 mm <br> Mech. <br> clearance 98 mm | TMTA 50 mm <br> Mech. <br> clearance 85 mm | TMTA 75 mm <br> Mech. clearance 85 mm | TMTA 75 mm <br> Mech. clearance 85 mm | TMTA 75 mm <br> Mech. clearance 85 mm | TMTA 50 mm |
| Acceptance - SET | $\begin{gathered} \text { "CW }<4700 \\ \text { mm Reduced } \\ \text { electrical } \\ \text { clearances } \end{gathered}$ | $\begin{gathered} \text { "CW }<4700 \\ \text { mm Reduced } \\ \text { electrical } \\ \text { clearances } \end{gathered}$ | $\begin{gathered} " C W<4700 \\ m m \end{gathered}$ | "CW<4700 <br> mm Reduced <br> electrical clearances | "CW<4700 <br> mm Reduced <br> electrical clearances | "CW<4700 <br> mm Reduced <br> electrical clearances | "CW<4700 <br> mm Reduced <br> electrical clearances | $\begin{gathered} \text { "CW }<4700 \\ \text { mm Reduced } \\ \text { electrical } \\ \text { clearances } \end{gathered}$ | ```CW<4700 mm Reduced electrical clearances``` |
| Derogation - SET | No | No | No | No | No | No | No | No | No |

### 5.2.3 Electrical Solutions requiring a derogation

A potential electrical solution for bridges where the contact wire height is less than 4400 mm but greater than 4200 mm is summarised in the tables below. A risk assessment has been undertaken for the solutions at each of these bridges and is contained in Appendix A of this report. In addition to this, a derogation would need to be sought for these bridges as the contact wire height is below minimum.

However, it has been required to develop compliant OHLE solutions with the minimum contact wire height for all the overbridges. Therefore, as indicated in section 6 of this report, further assessment for these bridges has been carried out in order to define the feasible options to improve the existing vertical clearance and to provide a compliant OHLE solution without requiring derogation.

NTA Vadess natsubust Impatr
larnród Éireann lrish Rail

ARUP

DART+
Coastal North

Table 5-8: Potential electrical solution with $4200 \mathrm{~mm}<\mathrm{CWH}<4400 \mathrm{~mm}$ (Derogation required)

|  | OBB39 | OBB44 | OBB55 | OBB78 | OBB81 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Current Structure Parameters |  |  |  |  |  |
| Structure Name | Rush \& Lusk Roadbridge | Tyrrelstown / Public Road | County Bridge / Public Road | Colpe Bridge / Public Road | MacBride Station |
| Chainage | 13 miles \& 1644 yards | 14 miles \& 1437 yards | 21 miles \& 304 yards | 30 miles \& 233 yards | 31 miles \& 1259 yards |
| Bridge Type | Roadbridge | Roadbridge | Roadbridge | Roadbridge | Footbridge |
| Is the Structure Listed | No | No | No | No | No (but located in a station which protected) |
| Width of Structure | 10.08 | 7.18 | 11.5 | 17.46 | 2.82 |
| Worst Vertical Clearance - TOR to Soffit | 4776 | 4585 | 4590 | 4680 | 4464 |
| Structure type | Flat | Flat | Flat | Flat | Flat |
| Bridge Constraints | Rush\&Lusk station | - |  |  | Drogheda MacBride Station |
| Potential OHLE solution | Contenary with zero encumbrance | Contenary with zero encumbrance | Contenary with zero encumbrance | Contenary with zero encumbrance | Contenary with zero encumbrance |

Table 5-9: Potential electrical solution parameters with CWH < 4400 mm (Derogation required)

|  | OBB39 | OBB44 | OBB55 | OBB78 | OBB81 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Potential OHLE solution | Contenary with zero encumbrance | Contenary with zero encumbrance | Contenary with zero encumbrance | Contenary with zero encumbrance | Contenary with zero encumbrance |
| OHLE Arrangement | Fitted with Elastic Bridge Arms | Free Running | Fitted with Elastic Bridge Arms | Fitted with Elastic Bridge Arms | Free Running |
| Static Clearance (Csc) - 1500Vdc | 100 | 100 | 100 | 100 | 100 |
| Dynamic Clearance (Cdc) 1500 Vdc | 80 | 80 | 80 | 80 | 80 |
| Minimum Position of the Contact Wire (considering tamping) | 4245 | 4215 | 4215 | 4193 | 4223 |
| Actual Design Contact Wire Height (Cdcl) (After Tamping) | 4370 | 4320 | 4270 | 4290 | 4270 |
| Maximum Design Contact Wire Height [Pre-Tamping] | 4420 | 4370 | 4270 | 4340 | 4270 |
| OHLE System Depth (Csd) | 0 | 0 | 0 | 0 | 0 |
| OHLE Uplift (Cwu) | 50 | 50 | 50 | 50 | 25 |
| OHLE Construction/ Installation (Cct) + Maintenance Tolerance (Cmt) | 50 | 30 | 30 | 30 | 30 |
| Structure Construction Tolerance (St) | 0 | 0 | 0 | 0 | 0 |

NTA

larnród Eireann lrish Rail

ARUP

OBB44
OBB39

| 50 | 50 | 0 | 50 | 0 |
| :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 5 | 0 | 5 |
| 25 | 25 | 5 | 25 | 5 |
| 12 | 12 | 12 | 10 | 10 |
| 25 | 25 | 25 | 17 | 17 |
| 5 | 5 | 5 | 5 | 5 |
| 4064 | 4064 | 4064 | 4064 | 4064 |
| 201 | 80 | 90 | 205 | 104 |
| 160km/h-100 mph | 160km/h-100 mph | 160km/h-100 mph | 160km/h-100 mph | 50km/h-30 mph |
| TMTA 50 mm | TMTA 50 mm <br> Mech. clearance 80 mm | Slab track <br> Mech. clearance 90 mm | TMTA 50 mm | Slab track <br> Mech. clearance 104 mm |
| CW<4700 mm | CW<4700 mm | CW<4700 mm | CW<4700 mm | $\mathrm{cW}<4700 \mathrm{~mm}$ <br> Reduced electrical clearances <br> OHLE construction + maintenance tolerance 30 mm <br> OHLE Uplift 25 mm |



OBB44 OBB55
OBB39 OBB44
CWH-4370 CWH-4320 Post tamping

- DART+

Coastal North

OBB78
OBB81

DART+
Coastal North

### 5.3 No Possible Electrical Solution

The bridges on the approach to Drogheda MacBride Station, namely the masonry arch bridges OBB80, OBB80A and OBB80B which carry McGrath's Lane over the railway line has insufficient clearance to provide an electrical only solution, even with a derogation.

However, it has been required to develop compliant OHLE solutions with the minimum contact wire height for all the overbridges. Therefore, as indicated in section 6 of this report, further assessment for these bridges has been carried out in order to define the feasible options to improve the existing vertical clearance and to provide a compliant OHLE solution without requiring derogation.

DART+
Coastal North

## 6. BRIDGES REQUIRING INTERVENTION

The following section identifies the bridges which have undergone further optioneering since PC1 to identify a preferred solution.

The bridges fall into two categories:

1. Bridges which have a potential electrical solution but would require a derogation.
2. Bridges with no viable electrical solution in the existing arrangement.

To avoid the need to apply for a derogation, options that consider lowering the track or modifying the bridges have been considered, as set out in the following sub-sections.

### 6.1 Bridges with an electrical solution requiring a derogation

### 6.1.1 OBB 39

As indicated previously, the current soffit height of this overbridge allows a non-compliant OHLE solution, with contact wire height lower than 4400 mm , as per Table 5-8 and Table 5-9, so additional options have had to be considered in order to achieve an OHLE compliant solution that does not require a derogation. These options are assessed in the Annex E1 Overbridge OBB39 Options Report. The preferred option entails local lowering of the track beneath the bridge to achieve an electrical clearance that does not require a derogation.

### 6.1.2 OBB 44

As indicated previously, the current soffit height of this overbridge allows a non-compliant OHLE solution, with contact wire height lower than 4400 mm , as per Table 5-8 and Table 5-9, so additional options have to be considered in order to achieve an OHLE compliant solution. These options are assessed in the Annex E2 Overbridge OBB44 Options Report. The preferred option entails local lowering of the track beneath the bridge to achieve an electrical clearance that does not require a derogation.

### 6.1.3 OBB 55

As indicated previously, the current soffit height of this overbridge allows a non-compliant OHLE solution, adopting the minimum contact wire height of 4270 mm and requiring a slab track, as per Table 5-8 and Table 5-9, so additional options have to be considered in order to achieve an OHLE compliant solution. These options are assessed in the Annex E3 Overbridge OBB55 Options Report. The preferred option entails local lowering of the track beneath the bridge to achieve an electrical clearance that does not require a derogation.

### 6.1.4 OBB 78

As indicated previously, the current soffit height of this overbridge allows a non-compliant OHLE solution, with contact wire height lower than 4400 mm , as per Table 5-8 and Table 5-9, so additional options have to be considered in order to achieve an OHLE compliant solution. These options are assessed in the Annex E4 Overbridge OBB78 Options Report. The preferred option entails local

DART+
Coastal North
lowering of the track beneath the bridge to achieve an electrical clearance that does not require a derogation.

### 6.1.5 OBB 81

As indicated previously, the current soffit height of this overbridge allows a non-compliant OHLE solution, adopting the minimum contact wire height of 4270 mm and requiring a slab track and a reduced OHLE uplift allowance of 25 mm , as per Table 5-8 and Table 5-9, so additional options have been considered in order to achieve an OHLE compliant solution. These options are assessed in the Annex E6 Overbridge OBB81 Options Report. The preferred option entails replacement of the bridge superstructure.

### 6.2 Bridges with no viable electrical solution in the existing arrangement

### 6.2.1 OBB80/80A/80B

As outlined above, the bridges on the approach to Drogheda MacBride Station, namely the masonry arch bridges OBB80, OBB80A and OBB80B which carry McGrath's Lane over the railway line has insufficient clearance to provide an electrical only solution, even with a derogation.

An infrastructure solution has been developed at this location - refer to Annex E5 - technical optioneering report for OBB80/80A/80B. This entails complete replacement of the bridge.

## Appendix A

Risk Assessments for Proposed Electrical Solutions where Contact Wire Height is less than 4700 mm .

## Risk Ranking Matrix

| Guidance for RISK RANKING MATRIX | Frequency (F) |  | Consequence (C) |  |  |  |  | Risk Classifications |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1 | 2 | 3 | 4 | 5 |  |
|  |  |  | Negligible | Minor | Major | Critical | Catastrophic |  |
|  | 5 | Frequent | 6 | 7 | 8 | 9 | 10 | 2-4 NEGLIGABLE LOW RISK: Ensure control measures are maintained and reviewed as necessary to control residual risk as far as is reasonably practicable. |
|  | 4 | Probable | 5 | 6 | 7 | 8 | 9 |  |
|  | 3 | Occasional | 4 | 5 | 6 | 7 | 8 | Control measures to reduce risk rating to a level which is as low as reasonably practicable (ALARP). Add details of residual risk to drawings/docs. |
|  | 2 | Remote | 3 | 4 | 5 | 6 | 7 |  |
|  | 1 | Improbable | 2 | 3 | 4 | 5 | 6 | 7-10 INTOLERABLE RISK: Activity not permitted. Hazard to be avoided or reduced |


| Frequency <br> Category | Classification <br> Term | Time <br> Frame | Midpoint <br> Frequency <br> Estimate | Description |
| :---: | :---: | :---: | :---: | :--- |
| 5 | Frequent | Less <br> than 1 | 1 in 6 <br> months | The event is likely to occur <br> frequently (probably on a |
| 4 | Probable | 1 year <br> to 10 <br> years | 1 in 5 years | The event will occur several <br> times and is likely to occur <br> often. |
| 3 | Occasional | 10 <br> years to <br> 100 <br> years | 1 in 50 <br> years | The event is likely to occur <br> several times. |
| 2 | 100 <br> years to <br> 1000 <br> years | 1 in 500 <br> years | The event can be expected <br> to occur during the lifecycle. |  |
| 1 | Improbable | 1000 <br> years or <br> greater | 1000 years | The event is unlikely to <br> occur, but may by exception <br> occur. |


| Consequence <br> Category | Classification <br> Term | Ratio | FWI <br> Equivalence | Description |
| :---: | :---: | :---: | :---: | :--- |
| 1 | Negligable | Minor | 5 <br> negliga | 0,005 |
| 2 | Major | 20 <br> minor | 0,1 | Non-reportable injury. |
| 3 | Critical | 10 <br> major <br> injuries. | 1 | Single fatality or multiple <br> major injuries, equivalent to <br> 1 Fatality Weighted Injury <br> (FWI). |
| 4 | Catastrophic | 5 <br> critical |  | Multiple fatalities. |
| 5 |  |  |  |  |

## Risk Ranking Matrix

| Guidance for RISK RANKING MATRIX | Frequency (F) |  | Consequence (C) |  |  |  |  | Risk Classifications |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1 | 2 | 3 | 4 | 5 |  |
|  |  |  | Negligible | Minor | Major | Critical | Catastrophic |  |
|  | 5 | Frequent | 6 | 7 | 8 | 9 | 10 | 2-4 NEGLIGABLE LOW RISK: Ensure control measures are maintained and reviewed as necessary to control residual risk as far as is reasonably practicable. |
|  | 4 | Probable | 5 | 6 | 7 | 8 | 9 |  |
|  | 3 | Occasional | 4 | 5 | 6 | 7 | 8 | Control measures to reduce risk rating to a level which is as low as reasonably practicable (ALARP). Add details of residual risk to drawings/docs. |
|  | 2 | Remote | 3 | 4 | 5 | 6 | 7 |  |
|  | 1 | Improbable | 2 | 3 | 4 | 5 | 6 | 7-10 INTOLERABLE RISK: Activity not permitted. Hazard to be avoided or reduced |


| Frequency <br> Category | Classification <br> Term | Time <br> Frame | Midpoint <br> Frequency <br> Estimate | Description |
| :---: | :---: | :---: | :---: | :--- |
| 5 | Frequent | Less <br> than 1 | 1 in 6 <br> months | The event is likely to occur <br> frequently (probably on a |
| 4 | Probable | 1 year <br> to 10 <br> years | 1 in 5 years | The event will occur several <br> times and is likely to occur <br> often. |
| 3 | Occasional | 10 <br> years to <br> 100 <br> years | 1 in 50 <br> years | The event is likely to occur <br> several times. |
| 2 | 100 <br> years to <br> 1000 <br> years | 1 in 500 <br> years | The event can be expected <br> to occur during the lifecycle. |  |
| 1 | Improbable | 1000 <br> years or <br> greater | 1000 years | The event is unlikely to <br> occur, but may by exception <br> occur. |


| Consequence <br> Category | Classification <br> Term | Ratio | FWI <br> Equivalence | Description |
| :---: | :---: | :---: | :---: | :--- |
| 1 | Negligable | Minor | 5 <br> negliga | 0,005 |
| 2 | Major | 20 <br> minor | 0,1 | Non-reportable injury. |
| 3 | Critical | 10 <br> major <br> injuries. | 1 | Single fatality or multiple <br> major injuries, equivalent to <br> 1 Fatality Weighted Injury <br> (FWI). |
| 4 | Catastrophic | 5 <br> critical |  | Multiple fatalities. |
| 5 |  |  |  |  |

## OBB33 DONABATE STATION ROADBRIDGE

| Approx. <br> Location | Miles | 11 |
| :--- | :---: | :---: |
| Yards | 727 |  |
| Soffit height | ${ }^{\sim} 5000 \mathrm{~mm}$ |  |
| Width | $12,19 \mathrm{~m}$ |  |
| Station | Y |  |
| Flat/arched | Flat |  |



## PROPOSED ELECTRICAL SOLUTION

Fitted contenary solution with zero encumbrance based on tolerances/allowances considered in hierarchy case 10 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \frac{5}{2} \\ & \hline \end{aligned}$ | Electrical clearance |  |  |  | Minimum soffit height (mm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB33 | 10 | Static EC | 4550 | 4411 | 25 | 14 | 50 | 0 | 25 | 20 | 30 | 0 | 0 | 0 | 150 | 5 | 120 | 0 | 4950 | ~5000 |
|  |  | Dynamic EC | 4550 | 4411 | 25 | 14 | 50 | 0 | 25 | 20 | 30 | 25 | 0 | 70 | 100 | 5 | 120 | 0 | 4995 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency (F) of occurrence of the event and the evaluation of the consequence (C) of the event in case it occurs. In both cases, they can be ranked from 1 (low likely of occurrence/low impact) to 5 (high likely/high impact). The risk evaluation (2 to 10) is obtained from the sum of both categories:

- Result 7 or higher: Intolerable risk
- Result 5 or 6: Tolerable risk
- Result 4 or lower: Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\vec{D}} \\ & \stackrel{y}{c} \end{aligned}$ | Safety Measures - mitigation description | F | C | 䔍 |
| Contact wire height < $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential, Electrocution | 4 | 4 | 8 | In the overbridge, proposed CWH is 4550 mm and spans are lower than 12 m , so minimum CWH will be 4411 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum (4190 mm ) given in the CME- TMS-327 Vehicle Gauging and in the FRS. In adjacent spans, span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case. | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\vec{y}} \\ & \stackrel{y}{c} \end{aligned}$ | Safety Measures - mitigation description | F | C | 䔍 |
| Contact wire height < $4700 \text { mm }$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Contact wire height < $4700 \text { mm }$ | Live parts of the OHLE or pantograph are closer to platform standing surface than minimum required | Electrocution | 4 | 4 | 8 | In the north side of the overbridge, the proposed adjacent spans are lower than 30 m , so considering pretamping CWH is 4600 mm , the minimum CWH will be 4453 mm . Pantograph depth is 210 mm and therefore minimum height for live parts is 4243 mm from ToR. Worst envelope situation is considering 60 mm cant towards platform and platform height in this section of 1070 mm from nearest rail, so minimum height of live parts from platform standing surface is 3162 mm . Therefore it fulfils the distance required in the EN50122-1 for 1500 V d.c. Cant and platform height values have been obtained from lidar surveys in Annex C of tender documentation. | 2 | 4 | 6 |

EVALUATION

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\vec{D}} \\ & \underset{\sim}{x} \end{aligned}$ | Safety Measures - mitigation description | F | C | 岂 |
| Insufficient load capacity of overbridge structure | Adding additional construction loads to structure | Instability and collapse of existing structure | 3 | 5 | 8 | Capacity of the overbridge will be checked in the following stages of the design | 1 | 5 | 6 |

OBB33A DONABATE FOOTBRIDGE

| Approx. | Miles | 11 |
| :--- | :---: | :---: |
| Location | Yards | 784 |
| Soffit height | $\sim 5100 \mathrm{~mm}$ |  |
| Width | $2,18 \mathrm{~m}$ |  |
| Station | Y |  |
| Flat/arched | Flat |  |



## PROPOSED ELECTRICAL SOLUTION

Free running solution with 100 mm minimum encumbrance based on tolerances/allowances considered in hierarchy case 6 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\frac{\#}{2}$ | : | U 0 0 0 0 0 0 0 0 0 |  |  | Minimum soffit height (mm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB33A | 6(*) | Static EC | 4600 | 4352 | 24 | 99 | 75 | 0 | 25 | 20 | 30 | 0 | 110 | 0 | 150 | 5 | 0 | 0 | 5015 | $\sim 5100$ |
|  |  | Dynamic EC | 4600 | 4352 | 24 | 99 | 75 | 0 | 25 | 20 | 30 | 25 | 110 | 110 | 100 | 5 | 0 | 0 | 5100 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency ( $F$ ) of occurrence of the event and the evaluation of the consequence (C) of the event in case it occurs. In both cases, they can be ranked from 1 (low likely of occurrence/low impact) to 5 (high likely/high impact). The risk evaluation ( 2 to 10) is obtained from the sum of both categories:

- Result 7 or higher: Intolerable risk
- Result 5 or 6: Tolerable risk
- Result 4 or lower: Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\stackrel{\rightharpoonup}{u}$ <br> $\stackrel{y}{4}$ <br>  | Safety Measures - mitigation description | F | C | 䔍 |
| Contact wire height < 4700 mm | Contact wire located closed to rolling stock than minimum required | Touch potential, Electrocution | 4 | 4 | 8 | In the overbridge, proposed CWH is 4600 mm and spans are lower than 12 m , so minimum CWH will be 4352 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum ( 4190 mm ) given in the CME- TMS-327 Vehicle Gauging and in the FRS. In adjacent spans, span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case. | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\stackrel{\stackrel{N}{\vec{W}}}{\stackrel{y}{c}}$ | Safety Measures - mitigation description | F | C | 若 |
| Contact wire height < $4700 \text { mm }$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Contact wire height < $4700 \text { mm }$ | Live parts of the OHLE or pantograph are closer to platform standing surface than minimum required | Electrocution | 4 | 4 | 8 | In the north side of the overbridge, the proposed adjacent spans are lower than 40 m , so considering pretamping CWH is 4675 mm , the minimum CWH will be 4502 mm . Pantograph depth is 210 mm and therefore minimum height for live parts is 4292 mm from ToR. Worst envelope situation is considering 60 mm of cant towards platform and platform height of 1060 mm from nearest rail, so minimum height of live parts from platform standing surface is 3221 mm . Therefore it fulfils the distance required in the EN50122-1 for 1500 V d.c. Cant and platform height values have been obtained from lidar surveys in Annex $C$ of tender documentation. | 2 | 4 | 6 |

OBB35 BEAVERSTOWN GOLF CLUB

| Approx. <br> Location | Miles | 12 |
| :--- | :---: | :---: |
|  | Yards | 445 |
| Soffit height | 4740 mm |  |
| Width | $4,54 \mathrm{~m}$ |  |
| Station | N |  |
| Flat/arched | Flat |  |



## PROPOSED ELECTRICAL SOLUTION

Free running contenary solution with zero encumbrance based on tolerances/allowances considered in hierarchy case 13 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  |  |  |  |  |  |  |  |  | CW and panto wear |  | $\frac{5}{2}$ |  |  |  |  | Minimum soffit height (mm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB35 | 13 | Static EC | 4400 | 4236 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 0 | 0 | 0 | 100 | 5 | 0 | 0 | 4655 | 4740 |
|  |  | Dynamic EC | 4400 | 4236 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 25 | 0 | 70 | 80 | 5 | 0 | 0 | 4730 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency ( $F$ ) of occurrence of the event and the evaluation of the consequence (C) of the event in case it occurs. In both cases, they can be ranked from 1 (low likely of occurrence/low impact) to 5 (high likely/high impact). The risk evaluation (2 to 10) is obtained from the sum of both categories:

- Result 7 or higher: Intolerable risk
- Result 5 or 6: Tolerable risk
- Result 4 or lower: Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\vec{訁}} \\ & \stackrel{y}{2} \end{aligned}$ | Safety Measures - mitigation description | F | C | 嶌 |
| Contact wire height < $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential, Electrocution | 4 | 4 | 8 | In the overbridge, proposed CWH is 4400 mm and spans are lower than 12 m , so minimum CWH will be 4236 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum (4190 mm ) given in the CME- TMS-327 Vehicle Gauging and in the FRS. In adjacent spans, span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case. | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\frac{\stackrel{\rightharpoonup}{\bar{y}}}{\substack{4 \\ \hline}}$ | Safety Measures - mitigation description |  | C | 若 |
| Contact wire height < $4700 \text { mm }$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Restricted electrical clearances of new OHLE at legacy structures, due to local route constraints. | Public use of legacy overbridges and structures with reduced electrical clearances. | Touch potential, Electrocution | 4 | 4 | 8 | Proposed OHLE solution considers static electrical clearance of 100 mm and dynamic electrical clearance of 80 mm , which are the minimum values according to I-ETR-4101 / Maintenance Parameters for 1500 Vdc OHLE; chapter 2.2 Electrical Clearances - subchapter 2.2.1 and FRS. <br> Additionally flashover protection could be also considered. | 2 | 4 | 6 |

## OBB38 ROGERSTOWN LANE

| Approx. Location | Miles | 13 |
| :---: | :---: | :---: |
|  | Yards | 999 |
| Soffit height |  | ~5020 mm |
| Width |  | 4,64 m |
| Station |  | N |
| Flat/arched |  | Arched |



## PROPOSED ELECTRICAL SOLUTION

Free running contenary solution with zero encumbrance based on tolerances/allowances considered in hierarchy case 13 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  |  |  |  |  |  |  |  |  | CW and panto wear |  | $\frac{5}{2}$ |  |  |  |  | Minimum soffit height (mm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB38 | 13 | Static EC | 4480 | 4316 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 0 | 0 | 0 | 100 | 5 | 0 | 200 | 4935 | $\sim 5020$ |
|  |  | Dynamic EC | 4480 | 4316 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 25 | 0 | 70 | 80 | 5 | 0 | 200 | 5010 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency（ $F$ ）of occurrence of the event and the evaluation of the consequence（C）of the event in case it occurs．In both cases，they can be ranked from 1 （low likely of occurrence／low impact）to 5 （high likely／high impact）．The risk evaluation（2 to 10）is obtained from the sum of both categories：
－Result 7 or higher：Intolerable risk
－Result 5 or 6：Tolerable risk
－Result 4 or lower：Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard－ <br> The unsafe act or condition． | Hazard Event <br> Description of the Hazard Event（the RISK）and the consequence． | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{⿹ ⿻}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures－mitigation description | F | C | 䔍 |
| Contact wire height＜ $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential，Electrocution | 4 | 4 | 8 | In the overbridge，proposed CWH is 4480 mm and spans are lower than 12 m ，so minimum CWH will be 4316 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum（4190 mm ）given in the CME－TMS－327 Vehicle Gauging and in the FRS． In adjacent spans，span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case． | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\stackrel{\stackrel{N}{\bar{y}}}{\substack{4 \\ \hline}}$ | Safety Measures - mitigation description | F | C | 若 |
| Contact wire height < $4700 \mathrm{~mm}$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Restricted electrical clearances of new OHLE at legacy structures, due to local route constraints. | Public use of legacy overbridges and structures with reduced electrical clearances. | Touch potential, Electrocution | 4 | 4 | 8 | Proposed OHLE solution considers static electrical clearance of 100 mm and dynamic electrical clearance of 80 mm , which are the minimum values according to I-ETR-4101 / <br> Maintenance Parameters for 1500 Vdc OHLE; chapter 2.2 Electrical Clearances - subchapter 2.2.1 and FRS. <br> Additionally flashover protection could be also considered. | 2 | 4 | 6 |

OBB38A RUSH \& LUSK FOOTBRIDGE

| Approx. | Miles | 13 |
| :--- | :---: | :---: |
| Location | Yards | 1564 |
| Soffit height | $\sim 5200 \mathrm{~mm}$ |  |
| Width | 3 m |  |
| Station | Y |  |
| Flat/arched | Flat |  |

PROPOSED ELECTRICAL SOLUTION

Free running solution with 300 mm of minimum encumbrance based on tolerances/allowances considered in hierarchy case 11 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  |  |  |  |  |  |  |  |  | CW and panto wear |  | $\begin{aligned} & \frac{\#}{2} \\ & \hline \end{aligned}$ | Electrical clearance | Survey tolerance |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB38A | 11(*) | Static EC | 4420 | 4221 | 18 | 56 | 75 | 0 | 25 | 20 | 30 | 0 | 320 | 0 | 150 | 5 | 0 | 0 | 5045 | 200 |
|  |  | Dynamic EC | 4420 | 4221 | 18 | 56 | 75 | 0 | 25 | 20 | 30 | 25 | 320 | 110 | 100 | 5 | 0 | 0 | 5130 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency（ $F$ ）of occurrence of the event and the evaluation of the consequence（C）of the event in case it occurs．In both cases，they can be ranked from 1 （low likely of occurrence／low impact）to 5 （high likely／high impact）．The risk evaluation（2 to 10）is obtained from the sum of both categories：
－Result 7 or higher：Intolerable risk
－Result 5 or 6：Tolerable risk
－Result 4 or lower：Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard－ <br> The unsafe act or condition． | Hazard Event <br> Description of the Hazard Event（the RISK）and the consequence． | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{⿹ ⿻}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures－mitigation description | F | C | 䔍 |
| Contact wire height＜ $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential，Electrocution | 4 | 4 | 8 | In the overbridge，proposed CWH is 4420 mm and span is lower than 30 m ，so minimum CWH will be 4221 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum（4190 mm ）given in the CME－TMS－327 Vehicle Gauging and in the FRS． In adjacent spans，span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case． | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C |  | Safety Measures - mitigation description | F | C |  |
| $\begin{aligned} & \text { Contact wire height < } \\ & 4700 \mathrm{~mm} \end{aligned}$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| $\begin{aligned} & \text { Contact wire height < } \\ & 4700 \mathrm{~mm} \end{aligned}$ | Live parts of the OHLE or pantograph are closer to platform standing surface than minimum required | Electrocution | 4 | 4 | 8 | In the south side of the overbridge, the proposed adjacent span is lower than 46 m , so considering pretamping CWH at the overbridge is 4495 mm and in the adjacent structure would 4575 mm , the minimum CWH will be 4333 mm . Pantograph depth is 210 mm and therefore minimum height for live parts is 4123 mm from ToR. Worst envelope situation is considering 10 mm cant away from platform and 1110 mm platform height from the nearest rail, so minimum height of live parts from platform standing surface is 3014 mm . Therefore it fulfils the distance required in the EN50122-1 for 1500 V d.c. Cant and platform height values have been obtained from lidar surveys in Annex C of tender documentation. | 2 | 4 | 6 |

OBB41

| Approx. | Miles | 14 |
| :--- | :---: | :---: |
| Location | Yards | 438 |
| Soffit height | 4703 mm |  |
| Width | $6,7 \mathrm{~m}$ |  |
| Station | N |  |
| Flat/arched | Flat |  |

## PROPOSED ELECTRICAL SOLUTION

Free running solution with contenary with zero encumbrance based on tolerances/allowances considered in hierarchy case 14 given in the Functional Requirement Spectification for DART+ Programme but with 4400 mm CW height.

|  |  |  |  |  |  |  |  |  |  |  |  | CW and panto wear |  | $\frac{5}{2}$ |  |  |  |  | Minimum soffit height (mm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB41 | 14 | Static EC | 4400 | 4261 | 25 | 14 | 50 | 0 | 25 | 20 | 30 | 0 | 0 | 0 | 100 | 5 | 0 | 0 | 4630 | 4703 |
|  |  | Dynamic EC | 4400 | 4261 | 25 | 14 | 50 | 0 | 25 | 20 | 30 | 25 | 0 | 50 | 80 | 5 | 0 | 0 | 4685 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency（ $F$ ）of occurrence of the event and the evaluation of the consequence（C）of the event in case it occurs．In both cases，they can be ranked from 1 （low likely of occurrence／low impact）to 5 （high likely／high impact）．The risk evaluation（2 to 10）is obtained from the sum of both categories：
－Result 7 or higher：Intolerable risk
－Result 5 or 6：Tolerable risk
－Result 4 or lower：Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard－ <br> The unsafe act or condition． | Hazard Event <br> Description of the Hazard Event（the RISK）and the consequence． | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{⿹ ⿻}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures－mitigation description | F | C | 䔍 |
| Contact wire height＜ $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential，Electrocution | 4 | 4 | 8 | In the overbridge，proposed CWH is 4400 mm and spans are lower than 12 m ，so minimum CWH will be 4261 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum（4190 mm ）given in the CME－TMS－327 Vehicle Gauging and in the FRS． In adjacent spans，span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case． | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\stackrel{ \pm}{3}$ <br> $\overrightarrow{y y}$ <br>  | Safety Measures - mitigation description | F | C | 䔍 |
| Contact wire height < $4700 \text { mm }$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Restricted electrical clearances of new OHLE at legacy structures, due to local route constraints. | Public use of legacy overbridges and structures with reduced electrical clearances. | Touch potential, Electrocution | 4 | 4 | 8 | Proposed OHLE solution considers static electrical clearance of 100 mm and dynamic electrical clearance of 80 mm , which are the minimum values according to I-ETR-4101 / Maintenance Parameters for 1500 Vdc OHLE; chapter 2.2 Electrical Clearances - subchapter 2.2.1 and FRS. <br> Additionally flashover protection could be also considered. | 2 | 4 | 6 |


| Approx. | Miles | 15 |
| :--- | :---: | :---: |
| Location | Yards | 856 |
| Soffit height | 4715 mm |  |
| Width | $4,81 \mathrm{~m}$ |  |
| Station | N |  |
| Flat/arched | Flat |  |



## PROPOSED ELECTRICAL SOLUTION

Free running solution with contenary with zero encumbrance based on tolerances/allowances considered in hierarchy case 13 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  |  |  |  |  |  |  | 弟 |  | CW and panto wear |  | $\frac{5}{2}$ |  |  |  |  | Minimum soffit height (mm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB45 | 13 | Static EC | 4400 | 4261 | 25 | 14 | 50 | 0 | 25 | 20 | 30 | 0 | 0 | 0 | 100 | 5 | 0 | 0 | 4630 | 4715 |
|  |  | Dynamic EC | 4400 | 4261 | 25 | 14 | 50 | 0 | 25 | 20 | 30 | 25 | 0 | 70 | 80 | 5 | 0 | 0 | 4705 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency（ $F$ ）of occurrence of the event and the evaluation of the consequence（C）of the event in case it occurs．In both cases，they can be ranked from 1 （low likely of occurrence／low impact）to 5 （high likely／high impact）．The risk evaluation（2 to 10）is obtained from the sum of both categories：
－Result 7 or higher：Intolerable risk
－Result 5 or 6：Tolerable risk
－Result 4 or lower：Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard－ <br> The unsafe act or condition． | Hazard Event <br> Description of the Hazard Event（the RISK）and the consequence． | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{⿹ ⿻}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures－mitigation description | F | C | 䔍 |
| Contact wire height＜ $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential，Electrocution | 4 | 4 | 8 | In the overbridge，proposed CWH is 4400 mm and spans are lower than 12 m ，so minimum CWH will be 4261 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum（4190 mm ）given in the CME－TMS－327 Vehicle Gauging and in the FRS． In adjacent spans，span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case． | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event Description of the Hazard Event (the RISK) and the consequence. | F | C | $\stackrel{ \pm}{3}$ <br> $\stackrel{y}{4}$ | Safety Measures - mitigation description | F | C | 芌 |
| $\begin{aligned} & \text { Contact wire height < } \\ & 4700 \mathrm{~mm} \end{aligned}$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Restricted electrical clearances of new OHLE at legacy structures, due to local route constraints. | Public use of legacy overbridges and structures with reduced electrical clearances. | Touch potential, Electrocution | 4 | 4 | 8 | Proposed OHLE solution considers static electrical clearance of 100 mm and dynamic electrical clearance of 80 mm , which are the minimum values according to I-ETR-4101 / <br> Maintenance Parameters for 1500 Vdc <br> OHLE; chapter 2.2 Electrical <br> Clearances - subchapter 2.2.1 and FRS. <br> Additionally flashover protection could be also considered. | 2 | 4 | 6 |

## OBB46 BALDONGAN

| Approx. | Miles | 16 |
| :--- | :---: | :---: |
| Location | Yards | 172 |
| Soffit height | $\sim 4860 \mathrm{~mm}$ |  |
| Width | $7,1 \mathrm{~m}$ |  |
| Station | N |  |
| Flat/arched | Flat |  |



## PROPOSED ELECTRICAL SOLUTION

Free running contenary solution with zero encumbrance based on tolerances/allowances considered in hierarchy case 10 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  |  |  |  |  |  |  |  |  | CW and panto wear |  | $\begin{aligned} & \frac{\#}{2} \\ & \hline \end{aligned}$ | Electrical clearance | Survey tolerance |  |  | Minimum soffit height (mm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB46 | 10 | Static EC | 4500 | 4336 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 0 | 0 | 0 | 150 | 5 | 0 | 0 | 4805 | $\sim 4860$ |
|  |  | Dynamic EC | 4500 | 4336 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 25 | 0 | 70 | 100 | 5 | 0 | 0 | 4850 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency（ $F$ ）of occurrence of the event and the evaluation of the consequence（C）of the event in case it occurs．In both cases，they can be ranked from 1 （low likely of occurrence／low impact）to 5 （high likely／high impact）．The risk evaluation（2 to 10）is obtained from the sum of both categories：
－Result 7 or higher：Intolerable risk
－Result 5 or 6：Tolerable risk
－Result 4 or lower：Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard－ <br> The unsafe act or condition． | Hazard Event <br> Description of the Hazard Event（the RISK）and the consequence． | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{⿹ ⿻}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures－mitigation description | F | C | 䔍 |
| Contact wire height＜ $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential，Electrocution | 4 | 4 | 8 | In the overbridge，proposed CWH is 4500 mm and spans are lower than 12 m ，so minimum CWH will be 4336 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum（4190 mm ）given in the CME－TMS－327 Vehicle Gauging and in the FRS． In adjacent spans，span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case． | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\begin{aligned} & \stackrel{ \pm}{\vec{y}} \\ & \stackrel{y}{c} \end{aligned}$ | Safety Measures - mitigation description | F | C | 䔍 |
| Contact wire height < 4700 mm | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |

OBB47 SKERRIES GOLF CLUB

| Approx. <br> Location | Miles | 16 |
| :--- | :---: | :---: |
| Yards | 1038 |  |
| Soffit height | 4900 mm |  |
| Width | $4,74 \mathrm{~m}$ |  |
| Station | N |  |
| Flat/arched | Arched |  |



## PROPOSED ELECTRICAL SOLUTION

Free running solution with 100 mm of minimum dropper based on tolerances/allowances considered in hierarchy case 9 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\frac{5}{2}$ |  |  |  |  |  | Actual soffit height (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB47 | 9 | Static EC | 4500 | 4223 | 27 | 125 | 75 | 0 | 25 | 20 | 30 | 0 | 0 | 0 | 150 | 5 | 0 | 0 | 4805 | 4900 |
|  |  | Dynamic EC | 4500 | 4223 | 27 | 125 | 75 | 0 | 25 | 20 | 30 | 25 | 0 | 110 | 100 | 5 | 0 | 0 | 4890 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency ( $F$ ) of occurrence of the event and the evaluation of the consequence (C) of the event in case it occurs. In both cases, they can be ranked from 1 (low likely of occurrence/low impact) to 5 (high likely/high impact). The risk evaluation ( 2 to 10) is obtained from the sum of both categories:

- Result 7 or higher: Intolerable risk
- Result 5 or 6: Tolerable risk
- Result 4 or lower: Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\vec{y}} \\ & \stackrel{y}{c} \end{aligned}$ | Safety Measures - mitigation description | F | C | $\xrightarrow{\stackrel{ \pm}{\vec{H}}}$ |
| $\begin{aligned} & \text { Contact wire height < } \\ & 4700 \mathrm{~mm} \end{aligned}$ | Contact wire located closed to rolling stock than minimum required | Touch potential, Electrocution | 4 | 4 | 8 | In the overbridge, proposed CWH is 4500 mm and spans are lower than 12 m , so minimum CWH will be 4223 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum (4190 mm ) given in the CME- TMS-327 Vehicle Gauging and in the FRS. <br> In adjacent spans, span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case. | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\begin{aligned} & \stackrel{ \pm}{\overrightarrow{\#}} \\ & \stackrel{y}{x} \end{aligned}$ | Safety Measures - mitigation description | F | C | 䔍 |
| Contact wire height < $4700 \text { mm }$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Restricted electrical clearances of new OHLE at legacy structures, due to local route constraints. | Public use of legacy overbridges and structures with reduced electrical clearances. | Touch potential, Electrocution | 4 | 4 | 8 | Proposed OHLE solution considers static electrical clearance of 100 mm and dynamic electrical clearance of 80 mm , which are the minimum values according to I-ETR-4101 / <br> Maintenance Parameters for 1500 Vdc OHLE; chapter 2.2 Electrical Clearances - subchapter 2.2.1 and FRS. <br> Additionally flashover protection could be also considered. | 2 | 4 | 6 |

OBB49 GOLF LINKS RD SKERRIES

| Approx. <br> Location | Miles | 17 |
| :--- | :---: | :---: |
|  | Yards | 524 |
| Soffit height | 4690 mm |  |
| Width | $7,42 \mathrm{~m}$ |  |
| Station | N |  |
| Flat/arched | Flat |  |



PROPOSED ELECTRICAL SOLUTION

Free running solution with contenary with zero encumbrance based on tolerances/allowances considered in hierarchy case 14 given in the Functional Requirement Spectification for DART+ Programme but with 4400 mm CW height.

|  |  |  |  |  |  |  |  |  |  |  |  | CW and panto wear |  | $\frac{5}{2}$ |  |  |  |  | Minimum soffit height (mm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB49 | 14 | Static EC | 4400 | 4275 | 16 | 9 | 50 | 0 | 25 | 20 | 30 | 0 | 0 | 0 | 100 | 5 | 0 | 0 | 4630 | 4690 |
|  |  | Dynamic EC | 4400 | 4275 | 16 | 9 | 50 | 0 | 25 | 20 | 30 | 25 | 0 | 50 | 80 | 5 | 0 | 0 | 4685 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency（ $F$ ）of occurrence of the event and the evaluation of the consequence（C）of the event in case it occurs．In both cases，they can be ranked from 1 （low likely of occurrence／low impact）to 5 （high likely／high impact）．The risk evaluation（2 to 10）is obtained from the sum of both categories：
－Result 7 or higher：Intolerable risk
－Result 5 or 6：Tolerable risk
－Result 4 or lower：Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard－ <br> The unsafe act or condition． | Hazard Event <br> Description of the Hazard Event（the RISK）and the consequence． | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{⿹ ⿻}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures－mitigation description | F | C | 䔍 |
| Contact wire height＜ $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential，Electrocution | 4 | 4 | 8 | In the overbridge，proposed CWH is 4400 mm and spans are lower than 12 m ，so minimum CWH will be 4275 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum（4190 mm ）given in the CME－TMS－327 Vehicle Gauging and in the FRS． In adjacent spans，span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case． | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\vec{y}} \\ & \cline { 1 - 2 } \end{aligned}$ | Safety Measures - mitigation description | F | C | 䔍 |
| Contact wire height < $4700 \mathrm{~mm}$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Restricted electrical clearances of new OHLE at legacy structures, due to local route constraints. | Public use of legacy overbridges and structures with reduced electrical clearances. | Touch potential, Electrocution | 4 | 4 | 8 | Proposed OHLE solution considers static electrical clearance of 100 mm and dynamic electrical clearance of 80 mm , which are the minimum values according to I-ETR-4101 / Maintenance Parameters for 1500 Vdc OHLE; chapter 2.2 Electrical Clearances - subchapter 2.2.1 and FRS. <br> Additionally flashover protection could be also considered. | 2 | 4 | 6 |

OBB51A SKERRIES FOOTBRIDGE

| Approx. <br> Location | Miles | 17 |
| :--- | :---: | :---: |
|  | Yards | 1708 |
| Soffit height | 4815 mm |  |
| Width | $2,25 \mathrm{~m}$ |  |
| Station | Y |  |
| Flat/arched | Flat |  |



PROPOSED ELECTRICAL SOLUTION

Free running contenary solution with zero encumbrance based on tolerances/allowances considered in hierarchy case 13 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  |  |  |  |  |  |  |  |  | CW and panto wear |  | $\frac{5}{2}$ |  |  |  |  | Minimum soffit height (mm) | 感 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB51A | 13 | Static EC | 4480 | 4316 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 0 | 0 | 0 | 100 | 5 | 0 | 0 | 4735 | 4815 |
|  |  | Dynamic EC | 4480 | 4316 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 25 | 0 | 70 | 80 | 5 | 0 | 0 | 4810 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency（ $F$ ）of occurrence of the event and the evaluation of the consequence（C）of the event in case it occurs．In both cases，they can be ranked from 1 （low likely of occurrence／low impact）to 5 （high likely／high impact）．The risk evaluation（2 to 10）is obtained from the sum of both categories：
－Result 7 or higher：Intolerable risk
－Result 5 or 6：Tolerable risk
－Result 4 or lower：Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard－ <br> The unsafe act or condition． | Hazard Event <br> Description of the Hazard Event（the RISK）and the consequence． | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{⿹ ⿻}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures－mitigation description | F | C | 䔍 |
| Contact wire height＜ $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential，Electrocution | 4 | 4 | 8 | In the overbridge，proposed CWH is 4480 mm and spans are lower than 12 m ，so minimum CWH will be 4316 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum（4190 mm ）given in the CME－TMS－327 Vehicle Gauging and in the FRS． In adjacent spans，span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case． | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\vec{y}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures - mitigation description | F | C | 䔍 |
| Contact wire height < $4700 \text { mm }$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Contact wire height < $4700 \text { mm }$ | Live parts of the OHLE or pantograph are closer to platform standing surface than minimum required | Electrocution | 4 | 4 | 8 | In the station the proposed adjacent spans are lower than 30 m , so considering pretamping CWH is 4555 mm , the minimum CWH will be 4431 mm . Pantograph depth is 210 mm and therefore minimum height for live parts is 4221 mm from ToR. <br> Worst point is 80 mm cant away from platform and platform height of 1165 mm from nearest rail, so minimum height of live parts from platform standing surface is 3060 mm . Therefore it fulfils the distance required in the EN50122-1 for 1500 V d.c. Cant and platform height values have been obtained from lidar surveys in Annex C of tender documentation. This distance has been compared with those of the latest overbridge survey and used the highest one. | 2 | 4 | 6 |


|  |  |  | VALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\stackrel{H}{\vec{訁}}$ | Safety Measures - mitigation description | F | C | $\stackrel{ \pm}{\overline{\#}}$ |
| Restricted electrical clearances of new OHLE at legacy structures, due to local route constraints. | Public use of legacy overbridges and structures with reduced electrical clearances. | Touch potential, Electrocution | 4 | 4 | 8 | Proposed OHLE solution considers static electrical clearance of 100 mm and dynamic electrical clearance of 80 mm , which are the minimum values according to I-ETR-4101 / <br> Maintenance Parameters for 1500 Vdc <br> OHLE; chapter 2.2 Electrical <br> Clearances - subchapter 2.2.1 and FRS. <br> Additionally flashover protection could be also considered. | 2 | 4 | 6 |

## OBB57A BALBRIGGAN FOOTBRIDGE

| Approx. Location | Miles | 21 |
| :---: | :---: | :---: |
|  | Yards | 1328 |
| Soffit height |  | 4775 mm |
| Width |  | 2,38 m |
| Station |  | Y |
| Flat/arched |  | Flat |



PROPOSED ELECTRICAL SOLUTION

Free running contenary solution with zero encumbrance based on tolerances/allowances considered in hierarchy case 13 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  |  |  |  |  |  |  |  |  | CW and panto wear |  | $\begin{aligned} & \frac{5}{2} \\ & \hline \end{aligned}$ | Electrical clearance |  |  |  | Minimum soffit height (mm) | 䦲 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB57A | 13 | Static EC | 4440 | 4276 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 0 | 0 | 0 | 100 | 5 | 0 | 0 | 4695 | 4775 |
|  |  | Dynamic EC | 4440 | 4276 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 25 | 0 | 70 | 80 | 5 | 0 | 0 | 4770 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency（ $F$ ）of occurrence of the event and the evaluation of the consequence（C）of the event in case it occurs．In both cases，they can be ranked from 1 （low likely of occurrence／low impact）to 5 （high likely／high impact）．The risk evaluation（2 to 10）is obtained from the sum of both categories：
－Result 7 or higher：Intolerable risk
－Result 5 or 6：Tolerable risk
－Result 4 or lower：Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard－ <br> The unsafe act or condition． | Hazard Event <br> Description of the Hazard Event（the RISK）and the consequence． | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{⿹ ⿻}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures－mitigation description | F | C | 䔍 |
| Contact wire height＜ $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential，Electrocution | 4 | 4 | 8 | In the overbridge，proposed CWH is 4440 mm and spans are lower than 12 m ，so minimum CWH will be 4276 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum（4190 mm ）given in the CME－TMS－327 Vehicle Gauging and in the FRS． In adjacent spans，span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case． | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\stackrel{N}{\bar{y}}$ | Safety Measures - mitigation description | F | C | 䔍 |
| Contact wire height < $4700 \text { mm }$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Contact wire height < $4700 \text { mm }$ | Live parts of the OHLE or pantograph are closer to platform standing surface than minimum required | Electrocution | 4 | 4 | 8 | In the station the proposed adjacent spans are lower than 30 m , so considering pretamping CWH is 4515 mm , the minimum CWH will be 4391 mm . Pantograph depth is 210 mm and therefore minimum height for live parts is 3512 mm from ToR. <br> Worst point is 80 mm cant away from platform and platform height of 1105 mm , so minimum height of live parts from platform standing surface is 3080 mm . Therefore it fulfils the distance required in the EN50122-1 for 1500 V d.c. Cant and platform height values have been obtained from lidar surveys in Annex C of tender documentation. This distance has been compared with those of the latest overbridge survey and used the highest one. | 2 | 4 | 6 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\begin{aligned} & \stackrel{H}{\vec{y}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures - mitigation description | F | C | 䔍 |
| Restricted electrical clearances of new OHLE at legacy structures, due to local route constraints. | Public use of legacy overbridges and structures with reduced electrical clearances. | Touch potential, Electrocution | 4 | 4 | 8 | Proposed OHLE solution considers static electrical clearance of 100 mm and dynamic electrical clearance of 80 mm , which are the minimum values according to I-ETR-4101 / <br> Maintenance Parameters for 1500 Vdc OHLE; chapter 2.2 Electrical Clearances - subchapter 2.2.1 and FRS. <br> Additionally flashover protection could be also considered. | 2 | 4 | 6 |

```
OBB62
```

| Approx. | Miles | 22 |
| :--- | :---: | :---: |
| Location | Yards | 1573 |
| Soffit height | $\sim 4880 \mathrm{~mm}$ |  |
| Width | $7,85 \mathrm{~m}$ |  |
| Station | N |  |
| Flat/arched | Flat |  |

## PROPOSED ELECTRICAL SOLUTION



Free running contenary solution with zero encumbrance based on tolerances/allowances considered in hierarchy case 10 given in the Functional Requirement Spectification for DART+ Programme


## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency（ $F$ ）of occurrence of the event and the evaluation of the consequence（C）of the event in case it occurs．In both cases，they can be ranked from 1 （low likely of occurrence／low impact）to 5 （high likely／high impact）．The risk evaluation（2 to 10）is obtained from the sum of both categories：
－Result 7 or higher：Intolerable risk
－Result 5 or 6：Tolerable risk
－Result 4 or lower：Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard－ <br> The unsafe act or condition． | Hazard Event <br> Description of the Hazard Event（the RISK）and the consequence． | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{⿹ ⿻}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures－mitigation description | F | C | 䔍 |
| Contact wire height＜ $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential，Electrocution | 4 | 4 | 8 | In the overbridge，proposed CWH is 4500 mm and spans are lower than 12 m ，so minimum CWH will be 4311 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum（4190 mm ）given in the CME－TMS－327 Vehicle Gauging and in the FRS． In adjacent spans，span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case． | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C |  | Safety Measures - mitigation description | F | C | $\xrightarrow{ \pm}$ |
| Contact wire height < 4700 mm | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |

## OBB63 -

| Approx. | Miles | 23 |
| :--- | :---: | :---: |
| Location | Yards | 866 |
| Soffit height | 4735 mm |  |
| Width | $4,47 \mathrm{~m}$ |  |
| Station | N |  |
| Flat/arched | Flat |  |



## PROPOSED ELECTRICAL SOLUTION

Free running contenary solution with zero encumbrance based on tolerances/allowances considered in hierarchy case 13 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  | $\qquad$ |  |  |  |  |  |  |  | CW and panto wear |  | $\begin{aligned} & 5 \\ & \frac{2}{2} \end{aligned}$ | Electrical clearance | Survey tolerance |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB63 | 13 | Static EC | 4400 | 4236 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 0 | 0 | 0 | 100 | 5 | 0 | 0 | 4655 | 4735 |
|  |  | Dynamic EC | 4400 | 4236 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 25 | 0 | 70 | 80 | 5 | 0 | 0 | 4730 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency（ $F$ ）of occurrence of the event and the evaluation of the consequence（C）of the event in case it occurs．In both cases，they can be ranked from 1 （low likely of occurrence／low impact）to 5 （high likely／high impact）．The risk evaluation（2 to 10）is obtained from the sum of both categories：
－Result 7 or higher：Intolerable risk
－Result 5 or 6：Tolerable risk
－Result 4 or lower：Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard－ <br> The unsafe act or condition． | Hazard Event <br> Description of the Hazard Event（the RISK）and the consequence． | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{⿹ ⿻}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures－mitigation description | F | C | 䔍 |
| Contact wire height＜ $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential，Electrocution | 4 | 4 | 8 | In the overbridge，proposed CWH is 4400 mm and spans are lower than 12 m ，so minimum CWH will be 4236 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum（4190 mm ）given in the CME－TMS－327 Vehicle Gauging and in the FRS． In adjacent spans，span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case． | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\frac{\stackrel{\rightharpoonup}{\bar{y}}}{\substack{4 \\ \hline}}$ | Safety Measures - mitigation description | F | C | 若 |
| Contact wire height < $4700 \text { mm }$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Restricted electrical clearances of new OHLE at legacy structures, due to local route constraints. | Public use of legacy overbridges and structures with reduced electrical clearances. | Touch potential, Electrocution | 4 | 4 | 8 | Proposed OHLE solution considers static electrical clearance of 100 mm and dynamic electrical clearance of 80 mm , which are the minimum values according to I-ETR-4101 / <br> Maintenance Parameters for 1500 Vdc OHLE; chapter 2.2 Electrical <br> Clearances - subchapter 2.2.1 and FRS. <br> Additionally flashover protection could be also considered. | 2 | 4 | 6 |

OBB66 GORMANSTOWN STATION ROADBRIDGE

| Approx. | Miles | 24 |
| :--- | :---: | :---: |
| Location | Yards | 19 |
| Soffit height | 4880 mm |  |
| Width | $4,52 \mathrm{~m}$ |  |
| Station | Y |  |
| Flat/arched | Flat |  |



PROPOSED ELECTRICAL SOLUTION

Free running contenary solution with zero encumbrance based on tolerances/allowances considered in hierarchy case 10 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  |  |  |  |  |  |  |  |  | CW and panto wear |  | $\frac{5}{2}$ | Electrical clearance |  |  |  | Minimum soffit height (mm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB66 | 10 | Static EC | 4525 | 4361 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 0 | 0 | 0 | 150 | 5 | 0 | 0 | 4830 | 4880 |
|  |  | Dynamic EC | 4525 | 4361 | 25 | 14 | 75 | 0 | 25 | 20 | 30 | 25 | 0 | 70 | 100 | 5 | 0 | 0 | 4875 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency（ $F$ ）of occurrence of the event and the evaluation of the consequence（C）of the event in case it occurs．In both cases，they can be ranked from 1 （low likely of occurrence／low impact）to 5 （high likely／high impact）．The risk evaluation（2 to 10）is obtained from the sum of both categories：
－Result 7 or higher：Intolerable risk
－Result 5 or 6：Tolerable risk
－Result 4 or lower：Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard－ <br> The unsafe act or condition． | Hazard Event <br> Description of the Hazard Event（the RISK）and the consequence． | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{⿹ ⿻}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures－mitigation description | F | C | 䔍 |
| Contact wire height＜ $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential，Electrocution | 4 | 4 | 8 | In the overbridge，proposed CWH is 4525 mm and spans are lower than 12 m ，so minimum CWH will be 4361 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum（4190 mm ）given in the CME－TMS－327 Vehicle Gauging and in the FRS． In adjacent spans，span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case． | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\stackrel{\stackrel{\rightharpoonup}{\bar{y}}}{\substack{4 \\ \hline}}$ | Safety Measures - mitigation description | F | C | 䔍 |
| Contact wire height < $4700 \text { mm }$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Contact wire height < $4700 \text { mm }$ | Live parts of the OHLE or pantograph are closer to platform standing surface than minimum required | Electrocution | 4 | 4 | 8 | In the station the proposed adjacent spans are lower than 45 m , so considering pretamping CWH is 4600 mm , the minimum CWH will be 4398 mm . Pantograph depth is 210 mm and therefore minimum height for live parts is 4188 mm from ToR. <br> Worst situation is considering 110 mm cant towards the platform and platform height is 1050 mm , so minimum height of live parts from platform standing surface is 3112 mm . Therefore it fulfils the distance required in the EN50122-1 for 1500 V d.c. Cant and platform height values have been obtained from lidar surveys in Annex C of tender documentation. This distance has been compared with those of the latest overbridge survey and used the highest one. | 2 | 4 | 6 |

## OBB66A(T GORMANSTOWN STATION FOOTBRIDGE (PLANNED)

| Approx. | Miles | 24 |
| :--- | :---: | :---: |
| Location | Yards | 120 |
| Soffit height | $\sim 5274 \mathrm{~mm}$ |  |
| Width | $2,55 \mathrm{~m}$ |  |
| Station | Y |  |
| Flat/arched | Flat |  |

## PROPOSED ELECTRICAL SOLUTION



Free running solution with 100 mm minimum encumbrance based on tolerances/allowances considered in hierarchy case 6 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  |  |  |  |  |  |  |  |  | CW and panto wear |  |  |  |  |  |  | Minimum soffit height (mm) | Actual soffit height (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB66A(TBC) | 6 | Static EC | 4645 | 4275 | 33 | 187 | 100 | 0 | 25 | 20 | 30 | 0 | 150 | 0 | 270 | 5 | 0 | 0 | 5245 | 5274 |
|  |  | Dynamic EC | 4645 | 4275 | 33 | 187 | 100 | 0 | 25 | 20 | 30 | 25 | 150 | 110 | 150 | 5 | 0 | 0 | 5260 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency ( $F$ ) of occurrence of the event and the evaluation of the consequence (C) of the event in case it occurs. In both cases, they can be ranked from 1 (low likely of occurrence/low impact) to 5 (high likely/high impact). The risk evaluation (2 to 10) is obtained from the sum of both categories:

- Result 7 or higher: Intolerable risk
- Result 5 or 6: Tolerable risk
- Result 4 or lower: Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | 䔍 | Safety Measures - mitigation description | F | C | 䔍 |
| Contact wire height < $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential, Electrocution | 4 | 4 | 8 | In the overbridge, proposed CWH is 4645 mm and spans are lower than 55 m , so minimum CWH will be 4275 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum (4190 mm ) given in the CME- TMS-327 Vehicle Gauging and in the FRS. In adjacent spans, span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case. | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\begin{aligned} & \stackrel{N}{\vec{y}} \\ & \underset{\sim}{x} \end{aligned}$ | Safety Measures - mitigation description | F | C | 若 |
| Contact wire height < $4700 \text { mm }$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Contact wire height < $4700 \text { mm }$ | Live parts of the OHLE or pantograph are closer to platform standing surface than minimum required | Electrocution | 4 | 4 | 8 | In the station the proposed adjacent spans are lower than 60 m , so considering pretamping CWH is 4745 mm , the minimum CWH will be 4436 mm . Pantograph depth is 210 mm and therefore minimum height for live parts is 4226 mm from ToR. <br> Worst situation is considering 110 mm cant towards the platform and platform height is 1050 mm , so minimum height of live parts from platform standing surface is 3150 mm . Therefore it fulfils the distance required in the EN50122-1 for 1500 V d.c. Cant and platform height values have been obtained from lidar surveys in Annex $C$ of tender documentation. This distance has been compared with those of the latest overbridge OBB66 survey and used the highest one. | 2 | 4 | 6 |

## OBB68 -

| Approx. | Miles | 24 |
| :--- | :---: | :---: |
| Location | Yards | 1757 |
| Soffit height | 4920 mm |  |
| Width | 6.55 m |  |
| Station | N |  |
| Flat/arched | Flat |  |



## PROPOSED ELECTRICAL SOLUTION

Free running contenary solution with zero encumbrance based on tolerances/allowances considered in hierarchy case 10 given in the Functional Requirement Spectification for DART+ Programme

|  |  |  |  | 荡 |  |  |  |  |  |  |  | CW and panto wear |  | $\begin{aligned} & 5 \\ & \frac{2}{2} \end{aligned}$ | Electrical clearance | Survey tolerance |  |  | Minimum soffit height (mm) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBB68 | 10 | Static EC | 4540 | 4351 | 25 | 14 | 100 | 0 | 25 | 20 | 30 | 0 | 0 | 0 | 150 | 5 | 0 | 0 | 4870 | 4920 |
|  |  | Dynamic EC | 4540 | 4351 | 25 | 14 | 100 | 0 | 25 | 20 | 30 | 25 | 0 | 70 | 100 | 5 | 0 | 0 | 4915 |  |

## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency（ $F$ ）of occurrence of the event and the evaluation of the consequence（C）of the event in case it occurs．In both cases，they can be ranked from 1 （low likely of occurrence／low impact）to 5 （high likely／high impact）．The risk evaluation（2 to 10）is obtained from the sum of both categories：
－Result 7 or higher：Intolerable risk
－Result 5 or 6：Tolerable risk
－Result 4 or lower：Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard－ <br> The unsafe act or condition． | Hazard Event <br> Description of the Hazard Event（the RISK）and the consequence． | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{⿹ ⿻}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures－mitigation description | F | C | 䔍 |
| Contact wire height＜ $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential，Electrocution | 4 | 4 | 8 | In the overbridge，proposed CWH is 4540 mm and spans are lower than 12 m ，so minimum CWH will be 4351 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum（4190 mm ）given in the CME－TMS－327 Vehicle Gauging and in the FRS． In adjacent spans，span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case． | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\vec{y}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures - mitigation description | F | C | 䔍 |
| Contact wire height < $4700 \text { mm }$ | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |

```
OBB77 -
```

| Approx. | Miles | 29 |
| :--- | :---: | :---: |
| Location | Yards | 1452 |
| Soffit height | ${ }^{\sim} 4850 \mathrm{~mm}$ |  |
| Width | $8,2 \mathrm{~m}$ |  |
| Station | N |  |
| Flat/arched | Flat |  |



PROPOSED ELECTRICAL SOLUTION

Fitted solution with zero encumbrance based on tolerances/allowances considered in hierarchy case 13 given in the Functional Requirement Spectification for DART+ Programme


## RISKS ASSESSMENT

The evaluation of risks considers the evaluation of the frequency（ $F$ ）of occurrence of the event and the evaluation of the consequence（C）of the event in case it occurs．In both cases，they can be ranked from 1 （low likely of occurrence／low impact）to 5 （high likely／high impact）．The risk evaluation（2 to 10）is obtained from the sum of both categories：
－Result 7 or higher：Intolerable risk
－Result 5 or 6：Tolerable risk
－Result 4 or lower：Negligible low risk

|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard－ <br> The unsafe act or condition． | Hazard Event <br> Description of the Hazard Event（the RISK）and the consequence． | F | C | $\begin{aligned} & \stackrel{\rightharpoonup}{\overline{⿹ ⿻}} \\ & \underset{\sim}{2} \end{aligned}$ | Safety Measures－mitigation description | F | C | 䔍 |
| Contact wire height＜ $4700 \text { mm }$ | Contact wire located closed to rolling stock than minimum required | Touch potential，Electrocution | 4 | 4 | 8 | In the overbridge，proposed CWH is 4400 mm and spans are lower than 12 m ，so minimum CWH will be 4261 mm according to the allowances and sag considered in the FRS and therefore higher than absolute minimum（4190 mm ）given in the CME－TMS－327 Vehicle Gauging and in the FRS． In adjacent spans，span lengths will be limited in order to maintain the CWH higher than 4190 mm in any case． | 1 | 4 | 5 |


|  |  |  | EVALUATION |  |  |  | EVALUATION |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hazard Cause | Hazard - <br> The unsafe act or condition. | Hazard Event <br> Description of the Hazard Event (the RISK) and the consequence. | F | C | $\stackrel{\stackrel{\rightharpoonup}{訁}}{\stackrel{y}{4}}$ | Safety Measures - mitigation description | F | C | 䔍 |
| Contact wire height < 4700 mm | Steep transition between nominal CWH and required CWH in the overbridge | Bad dynamic behaviour and quality of current collection. Increase of pantograph and contact wire wear. | 5 | 2 | 7 | Transition between different contact wire height will respect values given in the FRS. <br> These values are according to values indicated in Table 11 of EN50119 for required design speed. | 3 | 2 | 5 |
| Restricted electrical clearances of new OHLE at legacy structures, due to local route constraints. | Public use of legacy overbridges and structures with reduced electrical clearances. | Touch potential, Electrocution | 4 | 4 | 8 | Proposed OHLE solution considers static electrical clearance of 100 mm and dynamic electrical clearance of 80 mm , which are the minimum values according to I-ETR-4101 / Maintenance Parameters for 1500 Vdc OHLE; chapter 2.2 Electrical Clearances - subchapter 2.2.1 and FRS. <br> Additionally flashover protection could be also considered. | 2 | 4 | 6 |
| Insufficient load capacity of overbridge structure | Adding additional construction loads to structure | Instability and collapse of existing structure | 3 | 5 | 8 | Capacity of the overbridge will be checked in the following stages of the design | 1 | 5 | 6 |

## Appendix B

## Reports E1 to E6

Reports are as follows:

- E1- OBB39 Options Report
- E2- OBB44 Options Report
- E3- OBB55 Options Report
- E4- OBB78 Options Report
- E5- OBB80/80A/80B Options Report
- E6- OBB81 Options Report

